

SPECIFICATION

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POLY(ARYLENE ETHER)- POLYOLEFIN COMPOSITION AND ARTICLES DERIVED THEREFROM

Cross Reference to Related Applications

This application claims the benefit of U.S. Provisional Application Serial No. 60/258,691, filed December 28, 2000.

Background of Invention

- [0001] Compositions comprising poly(arylene ether)s and polyolefins are known in the art, and compositions further comprising specific impact modifiers and compatibilizing agents have been described.
- [0002] U.S. Patent No. 4,713,416 to Del Giudice et al. generally describes composition's comprising (a) a polyphenylene ether, (b) a thermoplastic polymer incompatible with the PPE, and (c) a polymeric compatibility-promoting agent comprising one or more blocks of vinylaromatic monomer units compatible with the polyphenylene ether (a) and one or more blocks of monomeric units of the same nature as the thermoplastic polymer (b) or compatible with that polymer.
- [0003] U.S. Patent No. 4,764,559 to Yamauchi et al. generally describes a composition comprising (a) a polyphenylene ether having a low degree of polymerization, with or without a styrene resin, (b) a polyolefin, and (c) a styrene compound/conjugated diene block copolymer or a hydrogenation product thereof.
- [0004] U.S. Patent No. 4,863,997 to Shibuya et al. generally describes a composition comprising (a) a polyolefin resin, (b) a polyphenylene ether resin, and (c) a

hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene that contains 45–80 weight percent of a repeating unit derived from the alkenyl aromatic compound.

- [0005] U.S. Patent No. 5,071,912 to Furuta et al. generally describes a composition comprising (a) a polyphenylene ether, (b) a styrene–modified propylene polymer or a composition containing a styrene–modified propylene polymer and polypropylene, and (c) at least two rubbery substances, one being compatible with (a) and the other incompatible with (a).
- [0006] U.S. Patent No. 5,081,187 to Maruyama et al. generally describes a composition comprising specific amounts of (a) a polyolefin, (b) a polyphenylene ether, (c) a partially hydrogenated alkenyl aromatic compound–isoprene block copolymer, and (d) an alkenyl aromatic compound–conjugated diene block copolymer.
- [0007] U.S. Patent No. 5,418,287 to Tanaka et al. generally describes a composition comprising (a) a polyphenylene ether, (b) a crystalline polyolefin resin, and (c) a graft copolymer where the backbone is a copolymer of (i) ethylene or at least one C_3-C_{12} alpha-olefin, and (ii) at least one chain nonconjugated diene.
- [0008] U.S. Patent No. 6,031,049 to Chino et al. generally describes a composition comprising specific amounts of (a) a component composed of syndiotactic polystyrene and a polyolefin, (b) a block or graft styrene–olefin copolymer having a styrene content of 40 to 85% by weight, and (c) a polyphenylene ether.
- [0009] European Patent Application No. 412,787 A2 to Furuta et al. generally describes compositions comprising (a) a polyphenylene ether, (b) a propylene polymer modified by grafting with a styrene–based monomer alone or in combination with another copolymerizable monomer, with or without an unmodified propylene polymer, and (c) a rubbery substance having chain A miscible with all or part of (a) and chain B miscible with all or part of (b).
- [0010] The commercial value of the above described compositions has been limited by deficiencies in the balance of properties such as stiffness, impact strength, and heat resistance, as well as the inconsistency of various properties from batch to batch and from molded sample to molded sample within the same batch. There remains a need

for poly(arylene ether)–polyolefin compositions having improved property balances. In particular, there remains a need for poly(arylene ether)–polyolefin compositions exhibiting improved balance between stiffness and impact strength. There also remains a need for poly(arylene ether)–polyolefin compositions exhibiting reduced batch-to-batch and sample-to-sample variability in key properties, including stiffness and impact strength.

Summary of Invention

[0011] The above-described and other drawbacks and disadvantages of the related art are alleviated by a thermoplastic composition, comprising: a poly(arylene ether); a poly(alkenyl aromatic) resin in an amount of at least about 30 weight percent of the total of the poly(arylene ether) and the poly(alkenyl aromatic) resin; a polyolefin; a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene.

[0012] Another embodiment of the invention is a thermoplastic composition comprising: a poly(arylene ether); a poly(alkenyl aromatic) resin; a polyolefin; a hydrogenated block copolymer of alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene and a polypropylene–polystyrene graft copolymer or an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene.

[0013] Other embodiments, including articles comprising reaction products of the above compositions, are described below.

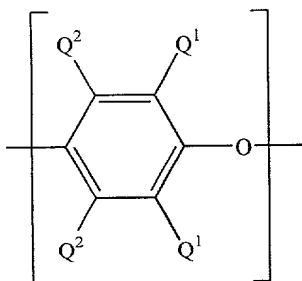
Detailed Description

[0014] A thermoplastic composition having an excellent balance of stiffness and impact strength, as well as reduced property variability, comprises: a poly(arylene ether); a poly(alkenyl aromatic) resin in an amount of at least about 30 weight percent of the total of the poly(arylene ether) and the poly(alkenyl aromatic) resin; a polyolefin; a

hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene.

[0015] The present inventors have surprisingly discovered that their compositions provide a substantial reduction in property variability compared to known compositions. The present compositions also provide a beneficial and previously unattainable balance between stiffness and impact strength. Other embodiments, including articles comprising the composition, are described below.

[0016] The composition may comprise any poly(arylene ether). The term poly(arylene ether) includes polyphenylene ether (PPE) and poly(arylene ether) copolymers; graft copolymers; poly(arylene ether) ether ionomers; and block copolymers of alkenyl aromatic compounds, vinyl aromatic compounds, and poly(arylene ether), and the like; and combinations comprising at least one of the foregoing; and the like. Poly(arylene ether)s are known polymers comprising a plurality of structural units of the formula



wherein for each structural unit, each Q^1 is independently halogen, primary or secondary C_1-C_8 alkyl, phenyl, C_1-C_8 haloalkyl, C_1-C_8 aminoalkyl, C_1-C_8 hydrocarboxy, or C_2-C_8 haloalkylhydrocarboxy wherein at least two carbon atoms separate the halogen and oxygen atoms; and each Q^2 is independently hydrogen, halogen, primary or secondary C_1-C_8 alkyl, phenyl, C_1-C_8 haloalkyl, C_1-C_8 aminoalkyl, C_1-C_8 hydrocarboxy, or C_2-C_8 haloalkylhydrocarboxy wherein at least two carbon atoms separate the halogen and oxygen atoms. Preferably, each Q^1 is alkyl or phenyl, especially C_{1-4} alkyl, and each Q^2 is independently hydrogen or methyl.

[0017] Both homopolymer and copolymer poly(arylene ether)s are included. The preferred homopolymers are those comprising 2,6-dimethylphenylene ether units. Suitable

copolymers include random copolymers comprising, for example, such units in combination with 2,3,6-trimethyl-1,4-phenylene ether units or copolymers derived from copolymerization of 2,6-dimethylphenol with 2,3,6-trimethylphenol. Also included are poly(arylene ether)s containing moieties prepared by grafting vinyl monomers or polymers such as polystyrenes, as well as coupled poly(arylene ether) in which coupling agents such as low molecular weight polycarbonates, quinones, heterocycles and formals undergo reaction in known manner with the hydroxy groups of two poly(arylene ether) chains to produce a higher molecular weight polymer. Poly(arylene ether)s of the present invention further include combinations of any of the above.

[0018] The poly(arylene ether) generally has a number average molecular weight of about 3,000 to about 40,000 atomic mass units (AMU) and a weight average molecular weight of about 20,000 to about 80,000 AMU, as determined by gel permeation chromatography. The poly(arylene ether) generally may have an intrinsic viscosity of about 0.2 to about 0.6 deciliters per gram (dL/g) as measured in chloroform at 25 ° C. Within this range, the intrinsic viscosity may preferably be up to about 0.5 dL/g, more preferably up to about 0.47 dL/g. Also within this range, the intrinsic viscosity may preferably be at least about 0.3 dL/g. It is also possible to utilize a high intrinsic viscosity poly(arylene ether) and a low intrinsic viscosity poly(arylene ether) in combination. Determining an exact ratio, when two intrinsic viscosities are used, will depend on the exact intrinsic viscosities of the poly(arylene ether)s used and the ultimate physical properties desired.

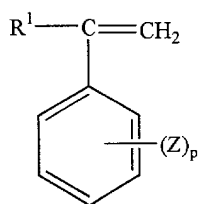
[0019] The poly(arylene ether)s are typically prepared by the oxidative coupling of at least one monohydroxyaromatic compound such as 2,6-xylenol or 2,3,6-trimethylphenol. Catalyst systems are generally employed for such coupling; they typically contain at least one heavy metal compound such as a copper, manganese or cobalt compound, usually in combination with various other materials.

[0020] Particularly useful poly(arylene ether)s for many purposes include those that comprise molecules having at least one aminoalkyl-containing end group. The aminoalkyl radical is typically located in an ortho position relative to the hydroxy group. Products containing such end groups may be obtained by incorporating an

appropriate primary or secondary monoamine such as di-n-butylamine or dimethylamine as one of the constituents of the oxidative coupling reaction mixture. Also frequently present are 4-hydroxybiphenyl end groups, typically obtained from reaction mixtures in which a by-product diphenoquinone is present, especially in a copper-halide-secondary or tertiary amine system. A substantial proportion of the polymer molecules, typically constituting as much as about 90% by weight of the polymer, may contain at least one of the aminoalkyl-containing and 4-hydroxybiphenyl end groups.

[0021] The composition may comprise poly(arylene ether) in an amount of about 10 to about 59 weight percent, based on the total weight of the composition. Within this range, it may be preferred to use a poly(arylene ether) amount of at least about 18 weight percent. Also within this range, it may be preferred to use a poly(arylene ether) amount of up to about 50 weight percent, more preferably up to about 40 weight percent.

[0022] The composition further comprises a poly(alkenyl aromatic) resin. The term "poly(alkenyl aromatic) resin" as used herein includes polymers prepared by methods known in the art including bulk, suspension, and emulsion polymerization, which contain at least 25% by weight of structural units derived from an alkenyl aromatic monomer of the formula



wherein R^1 is hydrogen, C_1-C_8 alkyl, halogen, or the like; Z is vinyl, halogen, C_1-C_8 alkyl, or the like; and p is 0 to 5. Preferred alkenyl aromatic monomers include styrene, chlorostyrenes such as p-chlorostyrene, and methylstyrenes such as p-methylstyrene. The poly(alkenyl aromatic) resins include homopolymers of an alkenyl aromatic monomer; random copolymers of an alkenyl aromatic monomer, such as styrene, with one or more different monomers such as acrylonitrile, butadiene, alpha-methylstyrene, ethylvinylbenzene, divinylbenzene and maleic anhydride; and rubber-modified poly(alkenyl aromatic) resins comprising blends and/or grafts of a rubber modifier and a homopolymer of an alkenyl aromatic monomer (as described above),

wherein the rubber modifier may be a polymerization product of at least one C_4-C_{10} nonaromatic diene monomer, such as butadiene or isoprene. The rubber-modified poly(alkenyl aromatic) resin may comprise about 98 to about 70 weight percent of the homopolymer of an alkenyl aromatic monomer and about 2 to about 30 weight percent of the rubber modifier. Within these ranges it may be preferred to use at least 88 weight percent of the alkenyl aromatic monomer. It may also be preferred to use up to about 94 weight percent of the alkenyl aromatic monomer. It may also be preferred to use at least 6 weight percent of the rubber modifier. It may also be preferred to use up to 12 weight percent of the rubber modifier.

[0023] The stereoregularity of the poly(alkenyl aromatic) resin may be atactic or syndiotactic. Highly preferred poly(alkenyl aromatic) resins include atactic and syndiotactic homopolystyrenes. Suitable atactic homopolystyrenes are commercially available as, for example, EB3300 from Chevron, and P1800 from BASF. Suitable syndiotactic homopolystyrenes are commercially available, for example, under the tradename QUESTRA[®] (e.g., QUESTRA[®] WA550) from Dow Chemical Company. Highly preferred poly(alkenyl aromatic) resins further include the rubber-modified polystyrenes, also known as high-impact polystyrenes or HIPS, comprising about 88 to about 94 weight percent polystyrene and about 6 to about 12 weight percent polybutadiene, with an effective gel content of about 10% to about 35%. These rubber-modified polystyrenes are commercially available as, for example, GEH 1897 from General Electric Plastics, and BA 5350 from Chevron.

[0024] The composition may comprise the poly(alkenyl aromatic) resin in an amount of about 4 to about 46 weight percent, with the proviso that the poly(alkenyl aromatic) resin constitutes at least about 30 weight percent, of the total of the poly(arylene ether) and the poly(alkenyl aromatic) resin. Within this range, it may be preferable to use the poly(alkenyl aromatic) resin in an amount of at least about preferably about 6 weight percent, based on the total weight of the composition.

[0025] In one embodiment, the amount of poly(alkenyl aromatic) resin may be expressed as a fraction of the total of poly(arylene ether) and poly(alkenyl aromatic) resin. The composition may preferably comprise poly(alkenyl aromatic) resin in an amount of about 30 to about 80 weight percent, based on the combined weight of poly(arylene

ether) and poly(alkenyl aromatic) resin. Within this range, it may be preferred to use a poly(alkenyl aromatic) resin amount up to about 70 weight percent, more preferably up to about 65 weight percent. Also within this range, it may be preferred to use a poly(alkenyl aromatic) resin amount of at least about 35 weight percent, more preferably at least about 40 weight percent. When the amount of poly(alkenyl aromatic) resin is less than about 30 weight percent of the total of the poly(arylene ether) and poly(alkenyl aromatic) resin, the composition after molding may be deficient in flexural modulus. When the amount of poly(alkenyl aromatic) resin is greater than about 80 weight percent of the total of the poly(arylene ether) and poly(alkenyl aromatic) resin, the composition after molding may be deficient in heat distortion temperature. The proportions of poly(alkenyl aromatic) resin and poly(arylene ether) may be manipulated to control the glass transition temperature (T_g) of the single phase comprising these two components relative to the T_g of the poly(arylene ether) alone, or relative to the melting temperature (T_m) of the polyolefin alone. For example, the relative amounts of poly(alkenyl aromatic) resin and poly(arylene ether) may be chosen so that the poly(arylene ether) and the poly(alkenyl aromatic) resin form a single phase having a glass transition temperature at least about 20 ° C greater, preferably at least about 30 ° C greater, than the glass transition temperature of the poly(alkenyl aromatic) resin alone, which may be, for example, about 100 ° C to about 110 ° C. Also, the relative amounts of poly(alkenyl aromatic) resin and poly(arylene ether) may be chosen so that the poly(arylene ether) and the poly(alkenyl aromatic) resin form a single phase having a glass transition temperature up to about 15 ° C greater, preferably up to about 10 ° C greater, more preferably up to about 1 ° C greater, than the T_m of the polyolefin alone. The relative amounts of poly(alkenyl aromatic) resin and poly(arylene ether) may be chosen so that the poly(arylene ether) and the poly(alkenyl aromatic) resin form a single phase having a glass transition temperature of about 130 ° C to about 180 ° C.

[0026]

The composition further comprises a polyolefin. The polyolefin may be a homopolymer or copolymer having at least about 80 weight percent of units derived from polymerization of ethylene, propylene, butylene, or a mixture thereof. Examples of polyolefin homopolymers include polyethylene, polypropylene, and polybutylene. Examples of polyolefin copolymers include random, graft, and block copolymers of

ethylene, propylene, and butylene with each other, and further comprising up to 20 weight percent of units derived from $C_5 - C_{10}$ alpha olefins (excluding aromatic alpha-olefins). Polyolefins further include blends of the above homopolymers and copolymers. Preferred polyolefins may have a flexural modulus of at least about 100,000 pounds per square inch (psi) at 23 ° C as measured according to ASTM D790. Suitable polyolefins may comprise, for example, the linear low density polyethylene available from ExxonMobil as LL-6201, the low density polyethylene available from ExxonMobil as LMA-027, the high density polyethylene available from ExxonMobil as HD-6605, the ultra-high molecular weight polyethylene available as Type 1900 from Montell Polyolefins, and the polybutylene (polybutene-1) available as PB0110 from Montell Polyolefins.

[0027] Presently preferred polyolefins include propylene polymers. The propylene polymer may be a homopolymer of polypropylene. Alternatively, the propylene polymer may be a random, graft, or block copolymer of propylene and at least one olefin selected from ethylene and $C_4 - C_{10}$ alpha-olefins (excluding aromatic alpha-olefins), with the proviso that the copolymer comprises at least about 80 weight percent, preferably at least about 90 weight percent, of repeating units derived from propylene. Blends of such propylene polymers with a minor amount of another polymer such as polyethylene are also included within the scope of propylene polymers. The propylene polymer may have a melt flow index of about 0.1 to about 50 g/10 min, preferably about 1 to about 30 g/10 min when measured according to ASTM D1238 at 2.16 kg and 200 ° C. The above-described propylene polymers can be produced by various known processes. Commercially available propylene polymers may also be employed.

[0028] Preferred propylene polymers include homopolypropylenes. Highly preferred propylene polymers include homopolypropylenes having a crystalline content of at least about 20%, preferably at least about 30%. Suitable isotactic polypropylenes are commercially available as, for example, PD403 pellets from Basell (formerly Montell Polyolefins of North America).

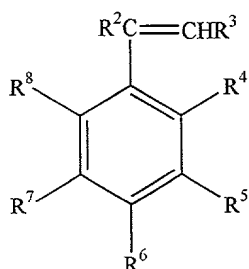
[0029] The composition may comprise polyolefin in an amount of about 10 to about 70 weight percent, preferably about 10 to about 60 weight percent, more preferably

about 10 to about 50 weight percent, based on the total weight of the composition.

[0030] The composition comprises a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene having an alkenyl aromatic content of about 40 to about 90 weight percent (hereinafter referred to as the "hydrogenated block copolymer"). The hydrogenated block copolymer is a copolymer comprising (A) at least one block derived from an alkenyl aromatic compound and (B) at least one block derived from a conjugated diene, in which the aliphatic unsaturated group content in the block (B) is reduced by hydrogenation. The arrangement of blocks (A) and (B) includes a linear structure, a grafted structure, and a radial teleblock structure with or without a branched chain.

[0031] Preferred among these structures are linear structures embracing diblock (A-B block), triblock (A-B-A block or B-A-B block), tetrablock (A-B-A-B block), and pentablock (A-B-A-B-A block or B-A-B-A-B block) structures as well as linear structures containing 6 or more blocks in total of A and B. More preferred are diblock, triblock, and tetrablock structures, with the A-B-A triblock structure being particularly preferred.

[0032] The alkenyl aromatic compound providing the block (A) is represented by formula



wherein R^2 and R^3 each independently represent a hydrogen atom, a C_1-C_8 alkyl group, a C_2-C_8 alkenyl group, or the like; R^4 and R^8 each independently represent a hydrogen atom, a C_1-C_8 alkyl group, a chlorine atom, a bromine atom, or the like; and R^5-R^7 each independently represent a hydrogen atom, a C_1-C_8 alkyl group, a C_2-C_8 alkenyl group, or the like, or R^4 and R^5 are taken together with the central aromatic ring to form a naphthyl group, or R^5 and R^6 are taken together with the central aromatic ring to form a naphthyl group.

[0033] Specific examples, of the alkenyl aromatic compounds include styrene, p-methylstyrene, alpha-methylstyrene, vinylxylenes, vinyltoluenes, vinylnaphthalenes,

divinylbenzenes, bromostyrenes, chlorostyrenes, and the like, and combinations comprising at least one of the foregoing alkenyl aromatic compounds. Of these, styrene, alpha-methylstyrene, p-methylstyrene, vinyltoluenes, and vinylxylenes are preferred, with styrene being more preferred.

[0034] Specific examples of the conjugated diene include 1,3-butadiene, 2-methyl-1,3-butadiene, 2,3-dimethyl-1,3-butadiene, 1,3-pentadiene, and the like. Preferred among them are 1,3-butadiene and 2-methyl-1,3-butadiene, with 1,3-butadiene being more preferred.

[0035] In addition to the conjugated diene, the hydrogenated block copolymer may contain a small proportion of a lower olefinic hydrocarbon such as, for example, ethylene, propylene, 1-butene, dicyclopentadiene, a non-conjugated diene, or the like.

[0036] The content of the repeating unit derived from the alkenyl aromatic compound in the hydrogenated block copolymer may be about 40 to about 90 weight percent, based on the total weight of the hydrogenated block copolymer. Within this range, the alkenyl aromatic compound content may preferably be at least about 50 weight percent, more preferably at least about 55 weight percent. Also within this range, the alkenyl aromatic compound content may preferably be up to about 85 weight percent, more preferably up to about 75 weight percent.

[0037] There is no particular limitation on the mode of incorporation of the conjugated diene in the hydrogenated block copolymer backbone. For example, when the conjugated diene is 1,3-butadiene, it may be incorporated with about 1% to about 99% 1,2-incorporation, with the remainder being 1,4-incorporation.

[0038] The hydrogenated block copolymer is preferably hydrogenated to such a degree that fewer than 50%, more preferably fewer than 20%, yet more preferably fewer than 10%, of the unsaturated bonds in the aliphatic chain moiety derived from the conjugated diene remain unreduced. The aromatic unsaturated bonds derived from the alkenyl aromatic compound may be hydrogenated to a degree of up to about 25%.

[0039] The hydrogenated block copolymer preferably has a number average molecular weight of about 5,000 to about 500,000 AMU, as determined by gel permeation

chromatography (GPC) using polystyrene standards. Within this range, the number average molecular weight may preferably be at least about 10,000 AMU, more preferably at least about 30,000 AMU, yet more preferably at least about 45,000 AMU. Also within this range, the number average molecular weight may preferably be up to about 300,000 AMU, more preferably up to about 200,000 AMU, yet more preferably up to about 150,000 AMU.

[0040] The molecular weight distribution of the hydrogenated block copolymer as measured by GPC is not particularly limited. The copolymer may have any ratio of weight average molecular weight to number average molecular weight.

[0041] Some of these hydrogenated block copolymers have a hydrogenated conjugated diene polymer chain to which crystallinity is ascribed. Crystallinity of the hydrogenated block copolymer can be determined by the use of a differential scanning calorimeter (DSC), for example, DSC-II Model manufactured by Perkin-Elmer Co. Heat of fusion can be measured by a heating rate of, for example, 10 ° C/min in an inert gas atmosphere such as nitrogen. For example, a sample may be heated to a temperature above an estimated melting point, cooled by decreasing the temperature at a rate of 10 ° C/min, allowed to stand for about 1 minute, and then heated again at a rate of 10 ° C/min.

[0042] The hydrogenated block copolymer may have any degree of crystallinity. In view of a balance of mechanical strength of the resulting resin composition, those hydrogenated block copolymers having a melting point of about -40 ° C to about 160 ° C or having no definite melting point (i.e., having non-crystallinity), as measured according to the above-described technique, are preferred. Within the melting point range of about -40 ° C to about 160 ° C, it may be preferred to use a hydrogenated block copolymer having a melting point of at least about -20 ° C, more preferably at least about 0 ° C, yet more preferably at least about 20 ° C, still more preferably at least about 40 ° C. Also within this range, it may be preferred to use a hydrogenated block copolymer having a melting point of up to about 140 ° C, more preferably up to about 110 ° C, yet more preferably up to about 100 ° C.

[0043] The hydrogenated block copolymer may have any glass transition temperature (T_g) ascribed to the hydrogenated conjugated diene polymer chain. From the

standpoint of low-temperature impact strength of the resulting resin composition, it preferably has a T_g of up to about -60°C , more preferably up to about -120°C . The glass transition temperature of the copolymer can be measured by the aforesaid DSC method or from the visco-elastic behavior toward temperature change as observed with a mechanical spectrometer.

[0044] Particularly preferred hydrogenated block copolymers are the styrene-(ethylene-butylene) diblock and styrene-(ethylene-butylene)-styrene triblock copolymers obtained by hydrogenation of styrene-butadiene and styrene-butadiene-styrene triblock copolymers, respectively.

[0045] The hydrogenated block copolymer may be synthesized by block polymerization followed by hydrogenation as described, for example, in U.S. Patent No. 4,863,997 to Shibuya et al. Suitable hydrogenated block copolymers include the styrene-(ethylene-butylene) diblock and styrene-(ethylene-butylene)-styrene triblock copolymers commercially available as, for example, TUFTEC[®] H1043 sold by Asahi Chemical.

[0046] The composition may comprise the hydrogenated block copolymer in an amount of about 1 to about 20 weight percent, preferably about 1 to about 15 weight percent, more preferably about 1 to about 12 weight percent, based on the total weight of the composition.

[0047] The composition further comprises an unhydrogenated block copolymer of alkenyl aromatic compound and a conjugated diene (referred to hereinafter as an "unhydrogenated block copolymer"). The unhydrogenated block copolymer is a copolymer comprising (A) at least one block derived from an alkenyl aromatic compound and (B) at least one block derived from a conjugated diene, in which the aliphatic unsaturated group content in the block (B) has not been reduced by hydrogenation. The alkenyl aromatic compound (A) and the conjugated diene (B) are defined in detail above in the description of the hydrogenated block copolymer. The arrangement of blocks (A) and (B) includes a linear structure and a so-called radial teleblock structure having a branched chain.

[0048] Preferred of these structures are linear structures embracing diblock (A-B block), triblock (A-B-A block or B-A-B block), tetrablock (A-B-A-B block), and pentablock (A-

B-A-B-A block or B-A-B-A-B block) structures as well as linear structures containing 6 or more blocks in total of A and B. More preferred are diblock, triblock, and tetrablock structures, with the A-B-A triblock structure being particularly preferred.

[0049] The unhydrogenated block copolymer may comprise about 10 to about 90 weight percent of the (A) blocks. Within this range, it may be preferred to use at least about 20 weight percent (A) blocks. Also within this range, it may be preferred to use up to about 80 weight percent (A) blocks.

[0050] Particularly preferred unhydrogenated block copolymers included styrene-butadiene-styrene triblock copolymers.

[0051] Suitable unhydrogenated block copolymers may be prepared by known methods or obtained commercially as, for example, KRATON[®] D series polymers, including KRATON[®] D1101 and D1102, from Kraton Polymers (formerly a division of Shell Chemical). Suitable unhydrogenated block copolymers further include the styrene-butadiene radial teleblock copolymers available as, for example, K-RESIN[®] KR01, KR03, KR05, and KR10 sold by Chevron Phillips Chemical Company.

[0052] The unhydrogenated block copolymers may be used at about 1 to about 20 weight percent, preferably about 1 to about 15 weight percent, more preferably about 1 to about 10 weight percent, of the total weight of the composition.

[0053] The composition may, optionally, further comprise a polypropylene-polystyrene graft copolymer. The polypropylene-polystyrene graft copolymer is herein defined as a graft copolymer having a propylene polymer backbone and one or more styrene polymer grafts.

[0054] The propylene polymer material that forms the backbone or substrate of the polypropylene-polystyrene graft copolymer is (a) a homopolymer of propylene; (b) a random copolymer of propylene and an olefin selected from the group consisting of ethylene and C₄-C₁₀ olefins, provided that, when the olefin is ethylene, the polymerized ethylene content is up to about 10 weight percent, preferably up to about 4 weight percent, and when the olefin is a C₄-C₁₀ olefin, the polymerized content of the C₄-C₁₀ olefin is up to about 20 weight percent, preferably up to about 16 weight percent; (c) a random terpolymer of propylene and at least two olefins selected

from the group consisting of ethylene and $C_4 - C_{10}$ alpha-olefins, provided that the polymerized $C_4 - C_{10}$ alpha-olefin content is up to about 20 weight percent, preferably up to about 16 weight percent, and, when ethylene is one of the olefins, the polymerized ethylene content is up to about 5 weight percent, preferably up to about 4 weight percent; or (d) a homopolymer or random copolymer of propylene which is impact-modified with an ethylene-propylene monomer rubber in the reactor as well as by physical blending, the ethylene-propylene monomer rubber content of the modified polymer being about 5 to about 30 weight percent, and the ethylene content of the rubber being about 7 to about 70 weight percent, and preferably about 10 to about 40 weight percent. The $C_4 - C_{10}$ olefins include the linear and branched $C_4 - C_{10}$ alpha-olefins such as, for example, 1-butene, 1-pentene, 3-methyl-1-butene, 4-methyl-1-pentene, 1-hexene, 3,4-dimethyl-1-butene, 1-heptene, 1-octene, 3-methyl-hexene, and the like. Propylene homopolymers and impact-modified propylene homopolymers are preferred propylene polymer materials. Although not preferred, propylene homopolymers and random copolymers impact modified with an ethylene-propylene-diene monomer rubber having a diene content of about 2 to about 8 weight percent also can be used as the propylene polymer material. Suitable dienes include dicyclopentadiene, 1,6-hexadiene, ethylidene norbornene, and the like.

[0055] The term "styrene polymer", used in reference to the grafted polymer present on the backbone of propylene polymer material in the polypropylene-polystyrene graft copolymer, denotes (a) homopolymers of styrene or of an alkyl styrene having at least one $C_1 - C_4$ linear or branched alkyl ring substituent, especially a p-alkyl styrene; (b) copolymers of the (a) monomers with one another in all proportions; and (c) copolymers of at least one (a) monomer with alpha-methyl derivatives thereof, e.g., alpha-methylstyrene, wherein the alpha-methyl derivative constitutes about 1 to about 40% of the weight of the copolymer.

[0056] The polypropylene-polystyrene graft copolymer will typically comprise about 10 to about 90 weight percent of the propylene polymer backbone and about 90 to about 10 weight percent of the styrene polymer graft. Within these ranges, the propylene polymer backbone may preferably account for at least about 20 weight percent, of the total graft copolymer; and the propylene polymer backbone may preferably account

for up to about 40 weight percent of the total graft copolymer. Also within these ranges, the styrene polymer graft may preferably account for at least about 50 weight percent, more preferably at least about 60 weight percent, of the total graft copolymer.

[0057] The preparation of polypropylene-polystyrene graft copolymers is described, for example, in U.S. Patent No. 4,990,558 to DeNicola, Jr. et al. Suitable polypropylene-polystyrene graft copolymers are also commercially available as, for example, P1045H1 and P1085H1 from Basell.

[0058] When present, the polypropylene-polystyrene graft copolymer may be used in an amount of about 0.5 to about 15 weight percent, preferably about 0.5 to about 10 weight percent, more preferably about 0.5 to about 8 weight percent, based on the total weight of the composition.

[0059] The composition may, optionally, further comprise an ethylene/alpha-olefin elastomeric copolymer. The alpha-olefin component of the copolymer may be at least one C₃-C₁₀ alpha-olefin. Preferred alpha-olefins include propylene, 1-butene, and 1-octene. The elastomeric copolymer may be a random copolymer having about 25 to about 75 weight percent ethylene and about 75 to about 25 weight percent alpha-olefin. Within these ranges, it may be preferred to use at least about 40 weight percent ethylene; and it may be preferred to use up to about 60 weight percent ethylene. Also within these ranges, it may be preferred to use at least about 40 weight percent alpha-olefin; and it may be preferred to use up to about 60 weight percent alpha-olefin. The ethylene/alpha-olefin elastomeric copolymer may typically have a melt flow index of about 0.1 to about 20 g/10 min at 2.16 kg and 200 °C, and a density of about 0.8 to about 0.9 g/ml.

[0060] Particularly preferred ethylene/alpha-olefin elastomeric copolymer rubbers include ethylene-propylene rubbers, ethylene-butene rubbers, ethylene-octene rubbers, and mixtures thereof.

[0061] The ethylene/alpha-olefin elastomeric copolymer may be prepared according to known methods or obtained commercially as, for example, the neat ethylene-propylene rubber sold as VISTALON® 878 by ExxonMobil Chemical and the ethylene-

butylene rubber sold as EXACT[®] 4033 by ExxonMobil Chemical. Ethylene/alpha-olefin elastomeric copolymers may also be obtained commercially as blends in polyolefins such as, for example, the ethylene-propylene rubber pre-dispersed in polypropylene sold as product numbers Profax 7624 and Profax 8023 from Basell, and the ethylene-butene rubber pre-dispersed in polypropylene sold as Catalloy K021P from Basell.

[0062] When present, the ethylene/alpha-olefin elastomeric copolymer may be used in an amount of about 1 to about 20 weight percent, based on the total weight of the composition. Within this range, it may be preferred to use an ethylene/alpha-olefin copolymer amount of at least about 3 weight percent. Also within this range, it may be preferred to use an ethylene/alpha-olefin copolymer amount of up to about 15 weight percent.

[0063] In one embodiment, the amount of ethylene/alpha-olefin elastomeric copolymer may be expressed as a fraction of the total of polyolefin and ethylene/alpha-olefin elastomeric copolymer. Thus, when the ethylene/alpha-olefin elastomeric copolymer is present, its amount may be expressed as about 1 to about 60 weight percent, on the combined weight of polyolefin and ethylene/alpha-olefin elastomeric copolymer. Within this range, it may be preferred to use at least about 10 weight percent of the ethylene/alpha-olefin copolymer. Also within this range, it may be preferred to use up to about 40 weight percent of the ethylene/alpha-olefin copolymer.

[0064] The composition may, optionally, further comprise a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 10 to less than 40 weight percent. For this component, the alkenyl aromatic compound and the conjugated diene compound are the same as those defined above for the hydrogenated block copolymer having an alkenyl aromatic content of 40 to about 90 weight percent. Such materials are commercially available as, for example, KRATON[®] G1650 and G1652 from Kraton Polymers. When present, the hydrogenated block copolymer having an alkenyl aromatic content of about 10 to less than 40 weight percent may be used at about 1 weight percent to about 20 weight percent, based on

the total weight of the composition.

[0065] In addition to the components described above, the composition may comprise one or more additives known in the art. Such additives may include, for example, stabilizers, mold release agents, processing aids, flame retardants, drip retardants, nucleating agents, UV blockers, dyes, pigments, particulate fillers (i.e., fillers having an aspect ratio less than about 3), reinforcing fillers, conductive fillers (e.g., conductive carbon black, and vapor grown carbon fibers having an average diameter of about 3 to about 500 nanometers), antioxidants, anti-static agents, blowing agents, and the like. Such additives are well known in the art and appropriate amounts may be readily determined.

[0066] In a preferred embodiment, the composition is substantially free of reinforcing fillers (i.e., the composition comprises less than 0.5 weight percent of reinforcing fillers, preferably less than 0.1 weight percent of reinforcing fillers, more preferably no intentionally added reinforcing fillers). For the purposes of this embodiment, a reinforcing filler is any material that is not soluble in either the poly(arylene ether)-containing phase or the polyolefin-containing phase, and which increases the flexural modulus of the composition.

[0067] In a preferred embodiment, the composition comprises: a poly(arylene ether); a poly(alkenyl aromatic) resin; a polyolefin; a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene; wherein the poly(arylene ether) and the poly(alkenyl aromatic) resin form a single phase having a glass transition temperature at least about 20 ° C greater than the glass transition temperature of the poly(alkenyl aromatic) resin alone.

[0068] In another preferred embodiment, the composition comprises: a poly(arylene ether); a poly(alkenyl aromatic) resin; a polyolefin; a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene; wherein the poly(arylene ether) and the poly(alkenyl aromatic)

resin form a single phase having a glass transition temperature no more than about 15 ° C greater than the melting temperature of the polyolefin alone.

[0069] In another preferred embodiment, the composition comprises: a poly(arylene ether); a poly(alkenyl aromatic) resin; a polyolefin; a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene; wherein the poly(arylene ether) and the poly(alkenyl aromatic) resin form a single phase having a glass transition temperature of about 130 ° C to about 180 ° C.

[0070] In another preferred embodiment, the composition comprises: a poly(arylene ether); a poly(alkenyl aromatic) resin; a polyolefin; a hydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene; and a polypropylene-polystyrene graft copolymer.

[0071] In another preferred embodiment, the composition comprises: about 10 to about 59 weight percent of a poly(arylene ether); about 3 to about 46 weight percent of a poly(alkenyl aromatic) resin, with the proviso that the poly(alkenyl aromatic) resin accounts for at least about 30 weight percent of the total of the poly(arylene ether) and the poly(alkenyl aromatic) resin; about 10 to about 40 weight percent of a polyolefin; about 1 to about 20 weight percent of a hydrogenated block copolymer of alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and about 1 to about 20 weight percent of an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene; wherein all weight percents are based on the total weight of the composition.

[0072] In another preferred embodiment, the composition comprises: about 10 to about 59 weight percent of a poly(arylene ether); about 1 to about 46 weight percent of a poly(alkenyl aromatic) resin; about 10 to about 40 weight percent of a polyolefin; about 1 to about 20 weight percent of a hydrogenated block copolymer of alkenyl

aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and about 1 to about 20 weight percent of an unhydrogenated block copolymer of an alkenyl aromatic compound and a conjugated diene; and about 0.5 to about 10 weight percent of a polypropylene-polystyrene graft copolymer; wherein all weight percents are based on the total weight of the composition.

[0073] In another preferred embodiment, the composition comprises: about 10 to about 59 weight percent of a poly(arylene ether); about 1 to about 46 weight percent of a poly(alkenyl aromatic) resin; about 1 to about 20 weight percent of an unhydrogenated block copolymer of alkenyl aromatic compound and a conjugated diene; about 10 to about 40 weight percent of a polyolefin; about 1 to about 20 weight percent of an ethylene/alpha-olefin elastomeric copolymer; about 1 to about 20 weight percent of a hydrogenated block copolymer of alkenyl aromatic compound and a conjugated diene, wherein the hydrogenated block copolymer has an alkenyl aromatic content of about 40 to about 90 weight percent; and about 0.5 to about 10 weight percent of a polypropylene-polystyrene graft copolymer; wherein all weight percents are based on the total weight of the composition.

[0074] As the composition is defined as comprising multiple components, it will be understood that each component is chemically distinct, particularly in the instance that a single chemical compound may satisfy the definition of more than one component.

[0075] The preparation of the compositions of the present invention is normally achieved by merely blending the ingredients under conditions for the formation of an intimate blend. Such conditions often include mixing in single or twin screw type extruders or similar mixing devices that can apply a shear to the components.

[0076] Preferred blending methods are described in detail in the co-filed U.S. Application Serial No. _____ [attorney docket number 08CN06031-2]. In a preferred embodiment, the components are blended in an extruder having at least two addition ports, with at least about 50%, preferably at least about 75%, more preferably all of the poly(arylene ether) added upstream, and at least about 50%, preferably at least about 75%, yet more preferably 100%, of the polyolefin added downstream. In another

preferred embodiment, the components are blended using at least two mixing stages, comprising upstream mixing and downstream mixing, wherein the upstream mixing is high-energy mixing characterized by at least two mixing elements and/or a mixing section not less than about 1 inch in length. Downstream mixing may be either high-energy mixing as described above or low-energy mixing, depending on the composition and desired properties of the composition.

[0077] The composition is suitable for the formation of articles or components of articles using a variety of molding techniques such as, for example, injection molding, blow molding, extrusion, sheet extrusion, film extrusion, profile extrusion, pultrusion, compression molding, thermoforming, pressure forming, hydroforming, vacuum forming, foam molding, and the like. The composition provides exceptional melt strength, making it especially suitable for the blow molding, thermoforming and extrusion processes.

[0078] The composition exhibits improved property balances. In particular, the composition exhibits an improved balance between stiffness and impact strength. For example the composition may exhibit a flexural modulus at 23 ° C, measured according to ASTM D790, of about 100 to at least about 350 kilopounds per square inch (kpsi), and a Dynatup Total Energy at 23 ° C, measured according to ASTM D3763, of about 0.5 to at least about 35 foot-pounds (ft-lb). Furthermore, at a given impact strength, the composition may provide high stiffness, and at a given stiffness, the composition may provide high impact strength.

[0079] The composition may exhibit low variability in properties, whether from batch-to-batch, or from sample-to-sample for a given batch. Variability may be calculated in percentage form as 100 times a property's standard deviation divided by the property's mean. The composition may exhibit batch-to-batch variability in Dynatup Total Energy at 23 ° C of less than about 15%, preferably less than about 10%. The composition may exhibit batch-to-batch variability in Flexural Modulus at 23 ° C of less than about 10 percent, preferably less than about 5%, more preferably less than about 3%. The composition may exhibit batch-to-batch variability in Izod Notched Impact Strength measured at 23 ° C according to ASTM D256 less than about 10%.

[0080] The invention is further illustrated by the following non-limiting examples.

EXAMPLES 1–20, COMPARATIVE EXAMPLE 1

[0081] Components utilized in the preparation of the thermoplastic composition are listed and described in Table 1.

[t1]

Table 1

Abbreviation	Description
PP, PD403	isotactic propylene polymer obtained as PD403 (pellet form) from Montell Polyolefin Inc.
PP, PH280	isotactic propylene polymer obtained as PH280 (particulate form) from Montell Polyolefin Inc.
EPR	Ethylene-propylene copolymer, obtained as VISTALON® 878 (pellet form) from ExxonMobil Chemical
EBR	Ethylene-butylene copolymer, obtained as EXACT® 4033 (pellet form) from ExxonMobil Chemical
PP-EPR, HECO-20	Polypropylene with ethylene-propylene rubber (EPR) as heterophasic/pre-dispersed, EPR content = 20 weight %, obtained as Profax 7624 (pellet form) from Montell Polyolefin Inc.
PP-EPR, HECO-30	Polypropylene with ethylene-propylene rubber (EPR) as heterophasic/pre-dispersed, EPR content = 30 weight %, obtained as Profax 7624 (pellet form) from Montell Polyolefin Inc.
PP-EBR, HECO-EBR	Polypropylene with ethylene-butene rubber (EBR) as heterophasic/pre-dispersed, EBR content = 60 weight %, obtained as ADFLEX® KS021P (pellet form) from Montell Polyolefin Inc.
PP-g-PS	Polypropylene-polystyrene graft copolymer, obtained as Interloy P1045H1 (pellet form) from Montell Polyolefin Inc.
PPE	poly(2,6-dimethylphenylene ether), intrinsic viscosity (IV) = 0.4 dl/g, obtained in powdered form from General Electric Company
xPS	homopolystyrene, obtained as Chevron EB3300 (pellet form) from Huntsman Chemical
HIPS	rubber-modified polystyrene having a polystyrene molecular weight of 230,000 g/mol and 10.3 weight% polybutadiene, obtained as GEH 1897 (pellet form) from General Electric Company
SBS	unhydrogenated styrene-butadiene-styrene triblock copolymer having about 31% polystyrene, obtained as KRATON® D1101 (pellet form) from Shell Chemical Company
SEBS G1652	hydrogenated styrene-butadiene-styrene triblock copolymer (also known as styrene-(ethylene-butadiene)-styrene triblock copolymer), 28 weight % polystyrene, obtained as KRATON® G1652 (pellet form) from Shell Chemical Company
SEBS H1043	hydrogenated styrene-butadiene-styrene triblock copolymer (also known as styrene-(ethylene-butadiene)-styrene triblock copolymer), 66 weight % polystyrene, obtained as TUFTEC® H1043 (pellet form) from Asahi Chemical

[0082]

General Blending/Compounding Procedure: Using quantities specified in Table 2, PP-g-PS, PPE, xPS, HIPS, SEBS, and SBS were hand mixed in a bag. Unless otherwise specified, all component amounts are expressed in parts by weight. The resulting

mixture was subsequently mixed aggressively with a mechanical blender for uniformity. The uniform mixture was subsequently fed through a feeder and entered into an extruder at the extruder initial entry point. In the instance when the quantity of the polystyrene or rubber-modified polystyrene components were each equal to or greater than 10% of the total blend weight, the polystyrene or rubber-modified polystyrene components were fed thorough a separate upstream feeder. Components PP and EPR or EBR, in quantities specified in Table 2, were fed downstream. The entry points were located after the feed throat, at approximately barrel 5 of a 10-barrel extruder.

[0083] General Extrusion: a 30 millimeter co-rotating twin-screw extruder was used. Blends were melt extruded at 520 ° F, 450–500 rpm, and a throughput rate of 30–55 pounds per hour. Melt from the extruder was forced through a three-hole die to produce melt strands. These strands were rapidly cooled by passing them through a cold-water bath. The cooled strands were chopped into pellets. Pellets were dried in an oven at 200 ° F for 2–4 hours.

[0084] General Molding: ASTM parts were molded on a 120 tonne molding machine (manufacturer Van Dorn) at 450–550 ° F barrel temperature and 100–120 ° F mold temperature.

[0085] Parts were tested according to ASTM methods. Izod notched impact was measured at 23 ° C and –30 ° C according to ASTM D256. Dynatup (falling dart) total energy and energy to failure were measured at 23 ° C and –30 ° C at 5 and 7.5 mph according to ASTM D3763. Heat distortion temperature (HDT) was measured at 66 psi and 264 psi on 1/8 inch samples according to ASTM D648. Flexural modulus and flexural strength at yield were measured at 23 ° C on 1/8 inch samples according to ASTM D790. Tensile strength at yield, tensile strength at break, and tensile elongation at break were measured at 23 ° C according to ASTM D638. Where presented, standard deviations reflect measurements on five samples.

[0086] The results are presented in Table 2. Formulations of the invention, represented by Examples 1–20, exhibit excellent balance of physical properties, especially their balance of impact strength and stiffness. Comparison of Example 19 and Comparative Example 1 illustrates the effect of the styrene content of the hydrogenated block

copolymer. Compared to Comparative Example 1, utilizing a hydrogenated block copolymer with 28 weight percent styrene, Example 19, utilizing a hydrogenated block copolymer with 66 weight percent styrene, exhibits superior ambient and low temperature impact strength (see, for example, "Notched Izod, 23 ° C", "Total Energy, 23 ° C, 7.5 mph", "Energy to Failure, 23 ° C, 7.5 mph", "Total Energy, -30 ° C, 7.5 mph"), superior stiffness (see, for example, "Flexural Modulus, 23 ° C" and "Flexural Strength at Yield"), superior tensile strength (see, for example, "Tensile Strength at Yield", "Tensile Strength at Break", and "Tensile Elongation at Break"), and dramatically reduced property variability (see standard deviations for all of above properties).
[t2]

Table 2.

	Ex. 1	Ex. 2	Ex. 3	Ex. 4
COMPOSITION				
PPE	21.00	18.00	25.20	18.00
xPS	14.00	12.00	0.00	0.00
HIPS	0.00	0.00	16.80	12.00
SBS D1101	15.00	5.00	10.33	5.00
SEBS H1043	10.00	10.00	5.33	10.00
SEBS G1652	0.00	0.00	0.00	0.00
PP-g-PS	10.00	6.67	5.33	10.00
PP	25.00	35.00	32.00	40.00
EBR	5.00	13.33	5.00	5.00
PROPERTIES				
HDT, 66psi, 1/8" (°F)	233.6	224.9	237.2	229.6
HDT, 66psi, 1/8", std dev (°F)	1.58	3.47	2.8	2.98
HDT, 264psi, 1/8" (°F)	166	153.1	159.3	152.4
HDT, 264psi, 1/8", std dev (°F)	2.72	2.16	0.68	1.1
Notched Izod, 23°C (ft-lb/in)	11.6	12.9	7.7	11.3
Notched Izod, 23°C, std dev (ft-lb/in)	0.4	0.3	0.4	0.4
Notched Izod, -30°C (ft-lb/in)	5.9	2.3	2.6	1.7
Notched Izod, -30°C, std dev (ft-lb/in)	0.6	0.3	0.1	0.1
Energy to Failure, 23°C, 7.5 mph (ft-lb)	18.06	17.21	18.05	18.15
Energy to Failure, 23°C, 7.5 mph, std dev (ft-lb)	0.57	0.91	0.39	0.38
Total Energy, 23°C, 7.5 mph (ft-lb)	28.59	30.14	27.39	31.17
Total Energy, 23°C, 7.5 mph, std dev (ft-lb)	0.88	0.91	1.85	0.77
Energy to Failure, -30°C, 7.5 mph (ft-lb)	22.34	22.05	15.02	20.89
Energy to Failure, -30°C, 7.5 mph, std dev (ft-lb)	0.55	0.47	6.90	6.76
Total Energy, -30°C, 7.5 mph (ft-lb)	33.11	34.6	16.63	29.17
Total Energy, -30°C, 7.5 mph, std dev (ft-lb)	1.73	2.93	8.49	11.00
Energy to Failure, -30°C, 5 mph (ft-lb)	22.54	22.78	17.92	23.77
Energy to Failure, -30°C, 5 mph, std dev (ft-lb)	0.46	0.39	6.53	0.36
Total Energy, -30°C, 5 mph (ft-lb)	33.94	37.82	21.15	35.19
Total Energy, -30°C, 5 mph, std dev (ft-lb)	0.88	2.28	9.38	0.42
Flexural Modulus, 23°C, 1/8" (psi)	195,900	177,100	195,200	190,500
Flexural Modulus, 23°C, 1/8", std dev (psi)	3,870	5,813	3,862	4,187
Flexural Strength at yield, 23°C, 1/8" (psi)	6,792	6,300	6,747	6,750
Flexural Strength at yield, 23°C, 1/8", std dev (psi)	53	155	44	85
Tensile Strength at yield, 23°C, (psi)	4,775	4,585	4,663	4,908
Tensile Strength at yield, 23°C, std dev (psi)	18.3	19.9	17.4	28.7
Tensile Strength at break, 23°C (psi)	5,119	4,962	4,812	4,750
Tensile Strength at break, 23°C, std dev (psi)	363	350	166	109
Tensile Elongation at break, 23°C (%)	265.04	367.7	231.3	311.4
Tensile Elongation at break, 23°C, std dev (%)	66.3	18.1	36.5	19.9

[t3]

Table 2. (cont.)

	Ex. 5	Ex. 6	Ex. 7	Ex. 8
COMPOSITION				
PPE	21.00	18.00	30.00	24.00
xPS	0.00	0.00	0.00	12.00
HIPS	14.00	12.00	20.00	4.00
SBS D1101	15.00	15.00	5.00	5.00
SEBS H1043	10.00	10.00	10.00	10.00
SEBS G1652	0.00	0.00	0.00	0.00
PP-g-PS	10.00	5.00	10.00	10.00
PP	25.00	20.00	20.00	20.00
EBR	5.00	20.00	5.00	15.00
PROPERTIES				
HDT, 66psi, 1/8" (°F)	221.7	195.4	252.7	245.3
HDT, 66psi, 1/8", std dev (°F)	0.80	6.19	3.27	2.16
HDT, 264psi, 1/8" (°F)	153.1	149.2	182.4	174.3
HDT, 264psi, 1/8", std dev (°F)	0.77	9.41	4.74	0.62
Notched Izod, 23°C (ft-lb/in)	11.9	12.7	8.9	11.9
Notched Izod, 23°C, std dev (ft-lb/in)	0.3	0.3	0.2	0.2
Notched Izod, -30°C (ft-lb/in)	7.4	14.2	2.5	4.7
Notched Izod, -30°C, std dev (ft-lb/in)	0.1	0.1	0.1	1.8
Energy to Failure, 23°C, 7.5 mph (ft-lb)	17.16	14.98	18.77	16.90
Energy to Failure, 23°C, 7.5 mph, std dev (ft-lb)	0.07	0.8	0.42	0.52
Total Energy, 23°C, 7.5 mph (ft-lb)	28.49	24.14	24.64	26.58
Total Energy, 23°C, 7.5 mph, std dev (ft-lb)	0.46	1.05	2.29	0.59
Energy to Failure, -30°C, 7.5 mph (ft-lb)	22.30	18.73	11.42	22.46
Energy to Failure, -30°C, 7.5 mph, std dev (ft-lb)	0.15	0.28	3.99	0.43
Total Energy, -30°C, 7.5 mph (ft-lb)	31.52	31.99	12.31	33.52
Total Energy, -30°C, 7.5 mph, std dev (ft-lb)	2.30	0.67	3.83	2.25
Energy to Failure, -30°C, 5 mph (ft-lb)	20.52	18.67	20.31	21.40
Energy to Failure, -30°C, 5 mph, std dev (ft-lb)	0.77	0.41	2.88	3.46
Total Energy, -30°C, 5 mph (ft-lb)	29.01	30.94	23.02	32.06
Total Energy, -30°C, 5 mph, std dev (ft-lb)	2.43	1.76	4.58	4.68
Flexural Modulus, 23°C, 1/8" (psi)	188,400	109,800	211,200	178,100
Flexural Modulus, 23°C, 1/8", std dev (psi)	1,704	1,407	1,360	1,476
Flexural Strength at yield, 23°C, 1/8" (psi)	6,721	4,013	7,748	6,546
Flexural Strength at yield, 23°C, 1/8", std dev (psi)	79	95	46	48
Tensile Strength at yield, 23°C (psi)	4,298	3,162	5,488	4,817
Tensile Strength at yield, 23°C, std dev (psi)	27.7	33.6	12.0	13.8
Tensile Strength at break, 23°C (psi)	5,057	4,499	5,257	4,834
Tensile Strength at break, 23°C, std dev (psi)	280	--	118	162
Tensile Elongation at break, 23°C (%)	338	400	146.7	185.8
Tensile Elongation at break, 23°C, std dev (%)	52	--	24	33

[t4]

Table 2. (cont.)

	Ex. 9	Ex. 10	Ex. 11	Ex. 12
COMPOSITION				
PPE	24.00	21.00	18.00	30.00
xPS	8.00	0.00	12.00	0.00
HIPS	8.00	14.00	0.00	20.00
SBS D1101	15.00	5.00	10.00	5.00
SEBS H1043	10.00	10.00	10.00	10.00
SEBS G1652	0.00	0.00	0.00	0.00
PP-g-PS	10.00	10.00	10.00	10.00
PP	20.00	20.00	20.00	20.00
EBR	5.00	20.00	20.00	5.00
PROPERTIES				
HDT, 66psi, 1/8" (°F)	237.4	222.2	221.0	248.6
HDT, 66psi, 1/8", std dev (°F)	0.16	1.69	6.41	0.36
HDT, 264psi, 1/8" (°F)	171.7	146.5	150.8	181.3
HDT, 264psi, 1/8", std dev (°F)	0.83	1.72	0.18	1.32
Notched Izod, 23°C (ft-lb/in)	10.7	12.6	13.4	9.5
Notched Izod, 23°C, std dev (ft-lb/in)	0.1	0.1	0.1	0.3
Notched Izod, -30°C (ft-lb/in)	6.6	12.5	12.9	3.0
Notched Izod, -30°C, std dev (ft-lb/in)	0.5	0.3	0.3	0.1
Energy to Failure, 23°C, 7.5 mph (ft-lb)	17.40	15.96	16.11	19.58
Energy to Failure, 23°C, 7.5 mph, std dev (ft-lb)	0.32	1.94	0.30	0.32
Total Energy, 23°C, 7.5 mph (ft-lb)	26.78	24.61	26.75	27.39
Total Energy, 23°C, 7.5 mph, std dev (ft-lb)	0.73	2.61	0.36	0.67
Energy to Failure, -30°C, 7.5 mph (ft-lb)	22.27	20.43	20.13	22.13
Energy to Failure, -30°C, 7.5 mph, std dev (ft-lb)	0.25	0.25	0.19	3.15
Total Energy, -30°C, 7.5 mph (ft-lb)	30.38	31.01	32.56	26.43
Total Energy, -30°C, 7.5 mph, std dev (ft-lb)	1.63	2.26	1.32	4.64
Energy to Failure, -30°C, 5 mph (ft-lb)	21.59	19.74	20.09	22.41
Energy to Failure, -30°C, 5 mph, std dev (ft-lb)	1.42	0.40	0.28	2.78
Total Energy, -30°C, 5 mph (ft-lb)	28.89	30.94	33.07	27.45
Total Energy, -30°C, 5 mph, std dev (ft-lb)	3.67	3.06	2.10	5.21
Flexural Modulus, 23°C, 1/8" (psi)	185,400	136,100	142,100	212,900
Flexural Modulus, 23°C, 1/8", std dev (psi)	500	1145	1515	2436
Flexural Strength at yield, 23°C, 1/8" (psi)	6,576	4,962	5,148	7,699
Flexural Strength at yield, 23°C, 1/8", std dev (psi)	28	65	52	29
Tensile Strength at yield, 23°C (psi)	4,718	3,918	3,854	5,405
Tensile Strength at yield, 23°C, std dev (psi)	24.6	14.8	14.6	17.7
Tensile Strength at break, 23°C (psi)	5,259	5,043	4,906	5,325
Tensile Strength at break, 23°C, std dev (psi)	339	133	110	85
Tensile Elongation at break, 23°C (%)	251.42	325.98	347.19	169.04
Tensile Elongation at break, 23°C, std dev (%)	49.7	22.1	31.6	17.0

[t5]

Table 2. (cont.)

	Ex. 13	Ex. 14	Ex. 15	Ex. 16
COMPOSITION				
PPE	25.20	18.00	18.00	27.00
PS	0.00	12.00	0.00	18.00
HIPS	16.80	0.00	12.00	0.00
SBS D1101	10.33	5.00	5.00	11.67
SEBS H1043	5.33	10.00	5.00	3.33
SEBS G1652	0.00	0.00	0.00	0.00
PP-g-PS	5.33	10.00	10.00	10.00
PP	32.00	40.00	30.00	20.00
EBR	5.00	5.00	20.00	10.00
PROPERTIES				
HDT, 66psi, 1/8" (°F)	240	238	209	251
HDT, 66psi, 1/8", std dev (°F)	2.88	1.53	5.22	2.80
HDT, 264psi, 1/8" (°F)	159	163.8	138.2	188.7
HDT, 264psi, 1/8", std dev (°F)	2.13	1.53	0.47	1.40
Notched Izod, 23°C (ft-lb/in)	6.9	10.6	11.3	7.3
Notched Izod, 23°C, std dev (ft-lb/in)	0.2	0.3	0.4	0.2
Notched Izod, -30°C (ft-lb/in)	2.7	0.9	5.7	2.3
Notched Izod, -30°C, std dev (ft-lb/in)	0.2	0.2	2.8	0.1
Energy to Failure, 23°C, 7.5 mph (ft-lb)	17.26	16.41	15.05	17.45
Energy to Failure, 23°C, 7.5 mph, std dev (ft-lb)	0.39	0.49	0.15	0.58
Total Energy, 23°C, 7.5 mph (ft-lb)	25.40	28.15	24.94	24.79
Total Energy, 23°C, 7.5 mph, std dev (ft-lb)	2.05	0.97	0.60	1.15
Energy to Failure, -30°C, 7.5 mph (ft-lb)	16.7	12.3	19.8	11.7
Energy to Failure, -30°C, 7.5 mph, std dev (ft-lb)	6.27	9.59	0.14	5.56
Total Energy, -30°C, 7.5 mph (ft-lb)	19.2	13.6	32.4	12.5
Total Energy, -30°C, 7.5 mph, std dev (ft-lb)	6.89	10.99	1.03	6.03
Energy to Failure, -30°C, 5 mph (ft-lb)	20.79	10.93	19.70	5.48
Energy to Failure, -30°C, 5 mph, std dev (ft-lb)	3.54	3.71	0.47	3.75
Total Energy, -30°C, 5 mph (ft-lb)	24.23	12.19	30.31	5.67
Total Energy, -30°C, 5 mph, std dev (ft-lb)	5.96	5.16	3.39	3.84
Flexural Modulus 23°C, 1/8" (psi)	193,400	216,500	146,600	221,400
Flexural Modulus, 23°C, 1/8", std dev (psi)	4,820	3,624	913	1,221
Flexural Strength at yield, 23°C, 1/8" (psi)	6,670	7,695	5,116	7,736
Flexural Strength at yield, 23°C, 1/8", std dev (psi)	58	119	53	29
Tensile Strength at yield, 23°C (psi)	4,700	5,232	3,836	5,196
Tensile Strength at yield, 23°C, std dev (psi)	11.3	51.2	18.8	15.5
Tensile Strength at break, 23°C (psi)	4,738	4,559	--	4,658
Tensile Strength at break, 23°C, std dev (psi)	186.0	128.9	--	40.7
Tensile Elongation at break, 23°C (%)	220.4	219.9	400.0	72.9
Tensile Elongation at break, 23°C, std dev (%)	27.72	46.95	--	9.96

[t6]

Table 2. (cont.)

	Ex. 17	Ex. 18	Ex. 19	Ex. 20
COMPOSITION				
PPE	30.96	27.56	16.20	30.96
PS	20.55	14.11	20.20	20.55
HIPS	0.00	4.26	0.00	0.00
SBS D1101	2.88	5.01	11.40	2.88
SEBS H1043	12.88	8.01	6.30	12.88
SEBS G1652	0.00	0.00	0.00	0.00
PP-g-PS	1.96	3.82	5.90	1.96
PP	27.15	24.23	33.90	27.15
EBR	3.63	13.00	6.20	3.63
PROPERTIES				
HDT, 66psi, 1/8" (°F)	259.7	256.0	229.0	259.7
HDT, 66psi, 1/8", std dev (°F)	--	0.41	1.8	--
HDT, 264psi, 1/8" (°F)	196.3	198.0	170.0	196.3
HDT, 264psi, 1/8", std dev (°F)	--	2.1	1.1	--
Notched Izod, 23°C (ft-lb/in)	6.6	10.6	8.9	6.6
Notched Izod, 23°C, std dev (ft-lb/in)	--	0.11	0.26	--
Notched Izod, -30°C (ft-lb/in)	3.8	6.8	2.5	3.8
Notched Izod, -30°C, std dev (ft-lb/in)	--	1.15	0.06	--
Energy to Failure, 23°C, 7.5 mph (ft-lb)	22.79	18.09	19.19	22.79
Energy to Failure, 23°C, 7.5 mph, std dev (ft-lb)	--	0.47	0.23	--
Total Energy, 23°C, 7.5 mph (ft-lb)	33.26	27.30	32.38	33.26
Total Energy, 23°C, 7.5 mph, std dev (ft-lb)	--	1.11	0.41	--
Energy to Failure, -30°C, 7.5 mph (ft-lb)	21.9	20.61	14.72	21.9
Energy to Failure, -30°C, 7.5 mph, std dev (ft-lb)	--	1.15	2.44	--
Total Energy, -30°C, 7.5 mph (ft-lb)	28.43	27.63	17.03	28.43
Total Energy, -30°C, 7.5 mph, std dev (ft-lb)	--	4.63	3.01	--
Energy to Failure, -30°C, 5 mph (ft-lb)	339.03	22.57	--	339.03
Energy to Failure, -30°C, 5 mph, std dev (ft-lb)	--	0.33	--	--
Total Energy, -30°C, 5 mph (ft-lb)	879.5	29.4	--	879.5
Total Energy, -30°C, 5 mph, std dev (ft-lb)	--	2.41	--	--
Flexural Modulus, 23°C, 1/8" (psi)	175,100	194,000	221,000	175,100
Flexural Modulus, 23°C, 1/8", std dev (psi)	--	153	1014	--
Flexural Strength at yield, 23°C, 1/8" (psi)	6,995	7,315	7,300	6,995
Flexural Strength at yield, 23°C, 1/8", std dev (psi)	--	51	32	--
Tensile Strength at yield, 23°C (psi)	5,566	5,153	5,060	5,566
Tensile Strength at yield, 23°C, std dev (psi)	--	17.14	19.00	--
Tensile Strength at break, 23°C (psi)	5,551	5,056	5,079	5,551
Tensile Strength at break, 23°C, std dev (psi)	--	31	65	--
Tensile Elongation at break, 23°C (%)	124.9	146.8	273.0	124.9
Tensile Elongation at break, 23°C, std dev (%)	--	6	12	--

[t7]

Table 2. (cont.)

	Comp. Ex. 1
COMPOSITION	
PPE	16.20
PS	20.20
HIIPS	0.00
SBS D1101	11.40
SEBS H1043	0.00
SEBS G1652	6.30
PP-g-PS	5.90
PP	33.90
EBR	6.20
PROPERTIES	
HDT, 66psi, 1/8" (°F)	226
<i>HDT, 66psi, 1/8", std dev (°F)</i>	--
HDT, 264psi, 1/8" (°F)	165.8
<i>HDT, 264psi, 1/8", std dev (°F)</i>	--
Notched Izod, 23°C (ft-lb/in)	5.1
<i>Notched Izod, 23°C, std dev (ft-lb/in)</i>	1.5
Notched Izod, -30°C (ft-lb/in)	2.6
<i>Notched Izod, -30°C, std dev (ft-lb/in)</i>	0.6
Energy to Failure, 23°C, 7.5 mph (ft-lb)	18.8
<i>Energy to Failure, 23°C, 7.5 mph, std dev (ft-lb)</i>	1.1
Total Energy, 23°C, 7.5 mph (ft-lb)	24.6
<i>Total Energy, 23°C, 7.5 mph, std dev (ft-lb)</i>	7.2
Energy to Failure, -30°C, 7.5 mph (ft-lb)	8
<i>Energy to Failure, -30°C, 7.5 mph, std dev (ft-lb)</i>	6.3
Total Energy, -30°C, 7.5 mph (ft-lb)	8.7
<i>Total Energy, -30°C, 7.5 mph, std dev (ft-lb)</i>	7
Energy to Failure, -30°C, 5 mph (ft-lb)	9
<i>Energy to Failure, -30°C, 5 mph, std dev (ft-lb)</i>	8.3
Total Energy, -30°C, 5 mph (ft-lb)	10.5
<i>Total Energy, -30°C, 5 mph, std dev (ft-lb)</i>	10.6
Flexural Modulus, 23°C, 1/8" (psi)	190,000
<i>Flexural Modulus, 23°C, 1/8", std dev (psi)</i>	15,900
Flexural Strength at yield, 23°C, 1/8" (psi)	6,429
<i>Flexural Strength at yield, 23°C, 1/8", std dev (psi)</i>	410
Tensile Strength at yield, 23°C (psi)	4,577
<i>Tensile Strength at yield, 23°C, std dev (psi)</i>	177
Tensile Strength at break, 23°C (psi)	4,333
<i>Tensile Strength at break, 23°C, std dev (psi)</i>	285
Tensile Elongation at break, 23°C (%)	155
<i>Tensile Elongation at break, 23°C, std dev (%)</i>	80

EXAMPLES 21–25

[0087]

Five example formulations including homopolystyrene but not rubber-modified polystyrene were prepared and tested according to the procedures described above. Results are presented in Table 3 and show excellent property balance.

[t8]

Table 3.

	Ex. 21	Ex. 22	Ex. 23	Ex. 24	Ex. 25
COMPOSITION					
PP	12.15	22.15	30.00	20.00	12.15
EPR	3.63	3.63	5.00	5.00	3.63
PP-g-PS	6.96	6.96	3.33	10.00	1.96
SBS	2.88	12.88	5.00	5.00	2.88
SEBS H1043	12.88	2.88	6.67	10.00	2.88
xPS	30.55	20.55	20.00	20.00	45.55
PPE	30.96	30.96	30.00	30.00	30.96
PROPERTIES					
Flexural Modulus, 23°C, 1/8" (psi)	228,100	231,700	247,700	260,100	350,400
Flexural Strength at yield, 23°C, 1/8" (psi)	8,629	8,183	9,012	9,498	12,840
HDT, 66psi, 1/8" (°F)	259.2	265.1	263.0	244.7	--
HDT, 264psi, 1/8" (°F)	213.7	202.6	195.8	199.6	221.3
Notched Izod, 23°C (ft-lb/in)	7.6	2.9	5.6	7.7	1.7
Notched Izod, -30°C (ft-lb/in)	2.6	1.5	1.1	0.9	0.9
Unnotched Izod, 23°C, 1/8" (ft-lb/in)	31.0	34.4	--	--	12.9
Energy to Failure, 23°C, 7.5 mph (ft-lb)	33.7	26.7	20.5	18.8	2.9
Total Energy, 23°C, 7.5 mph (ft-lb)	20.25	3.98	31.25	27.34	3.69
Energy to Failure, -30°C, 7.5 mph (ft-lb)	27.86	4.26	3.06	1.53	0.73
Total Energy, -30°C, 7.5 mph (ft-lb)	17.47	1.50	3.27	1.66	0.92
Energy to Failure, -30°C, 5 mph (ft-lb)	19.81	1.64	6.47	1.69	8.29
Total Energy, -30°C F, 5 mph (ft-lb)	20.69	1.48	6.70	1.79	132.1
Tensile Strength at yield, 23°C (psi)	6,046	5,597	6,178	6,389	8,701
Tensile Stress at break, 23°C (psi)	5,797	5,487	5,382	5,500	6,938
Tensile Elongation at break, 23°C (%)	83.07	26.19	120.26	92.29	20.84

EXAMPLES 26-28, COMPARATIVE EXAMPLES 2-4

[0088]

These examples and comparative examples illustrate the advantage of the invention in reducing batch-to-batch and sample-to-sample property variability. Samples were formulated and tested as described above. Examples 26-28 represent three different batches having the composition shown for Example 19 in Table 2, above, utilizing a hydrogenated block copolymer having a styrene content of 66%. Comparative Examples 2-4 represent three different batches having the composition shown for Comparative Example 1 in Table 2, above, utilizing a hydrogenated block copolymer having a styrene content of 28%. Property results are given in Table 4. The results show that batch-to-batch variations in properties, especially impact strength properties, are consistently and substantially lower for the formulations of Examples 26-28 compared to the formulations of Comparative Examples 2-4.

[t9]

[110]

Table 4

	no of samples	Comp Ex. 2	Comp Ex. 3	Comp Ex. 4	Mean for C. Exs. 2-4	std dev for C. Exs. 2-4	Ex. 26	Ex. 27	Ex. 28	Mean for Exs 26-28	std dev for Exs 26-28
HDT @ 66psi, 1/8" (°F)	3	228.3	221	228.7	226	4.3	230.9	229.4	227.3	229	1.8
std dev		3.95	1.25	2.03			2.61	1.23	1.41		
HDT @ 264psi, 1/8" (°F)	3	169.3	161.9	166.1	166	3.7	171.1	170.1	168.9	170	1.1
std dev		0.55	2.97	1.73			2.25	3.65	1.01		
Notched Izod, 23°C (ft-lb/in)	5	4.2	6.9	4.3	5.1	1.5	8.7	8.8	9.2	8.9	0.3
std dev		0.1	0.2	0.2			0.4	0.5	0.2		
Notched Izod, -30°C (ft-lb/in)	5	2.1	3.3	2.3	2.6	0.6	2.5	2.4	2.5	2.5	0.1
std dev		0.2	0.1	0.2			0.1	0.1	0.1		
Energy to Failure, 23°C, 7.5mph (ft-lb)	5	17.53	19.59	19.42	18.8	1.1	19.07	19.46	19.04	19.2	0.2
std dev		2.17	0.28	0.42			0.16	0.33	0.21		
Total Energy, 23°C, 7.5mph (ft-lb)	5	18.31	32.41	23.15	24.6	7.2	32.68	31.91	32.54	32.4	0.4
std dev		2.3	1.68	2.11			1.22	1.86	0.59		
Energy to Failure, -30°C, 7.5mph (ft-lb)	5	3.23	15.13	5.68	8.0	6.3	12.71	14.01	17.43	14.7	2.4
std dev		1	8.84	3.55			8.74	5.86	6.61		
Total Energy, -30°C, 7.5mph (ft-lb)	5	3.43	16.63	5.95	8.7	7.0	14.24	16.63	20.22	17.0	3.0
std dev		1.04	10.08	3.67			10.45	9.92	9.33		
Energy to Failure, -30°C, 5mph (ft-lb)	5	2.64	18.4	5.99	9.0	8.3	20.81	22.22	22.79	21.9	1.0
std dev		2.45	7	4.58			2.87	0.28	0.32		
Total Energy, -30°C, 5mph (ft-lb)	5	2.77	22.69	6.18	10.5	10.7	26.82	27.26	34.66	29.6	4.4
std dev		2.52	10.66	4.66			7.32	4.08	4.15		
Flexural Modulus, 23°C, 1/8" (kpsi)	3	203.3	173.3	194.2	190	16	221.4	220.7	219.4	221	1
std dev		1.642	1.006	2.747			1.117	1.317	1.881		

This example and these comparative examples collectively illustrate the advantages of the composition in molding applications requiring high melt strength. The Example 29 formulation consisted of 27.6 weight percent PE, 14.1 weight percent XPS, 4.3 weight percent HIPS, 5.0 weight percent SBS, 8.0 weight percent SEBS,

EXAMPLE 29, COMPARATIVE EXAMPLES 5-10

Table 4 (cont.)

	no. of samples	Comp. Ex. 2	Comp. Ex. 3	Comp. Ex. 4	Mean for C Exs. 2-4	std dev for C Exs. 2-4	Ex. 26	Ex. 27	Ex. 28	Mean for Exs. 26-28	std dev for Exs. 26-28
Flexural Strength at yield, 23°C, 1/8" (psi)	3	6,775	5,976	6,537	6,429	410	7,336	7,275	7,290	7,300	32
std dev.		22	31	56			32	20	11		
Tensile Strength at yield, 23°C, 2m/min (psi)	5	4,731	4,383	4,616	4,577	177	5,077	5,063	5,039	5,060	19
std dev		6.35	20.8	23.2			0	10.2	10.2		
Tensile Strength at break, 23°C, 2m/min (psi)	5	4,203	4,660	4,136	4,333	285	5,154	5,036	5,047	5,079	65
std dev		63.5	87	48			0	121	20		
Tensile Elongation at break, 23°C, 2m/min (%)	5	91	247.77	125.17	155	82	277.22	259.83	281.98	273	12
std dev		16	12	7.8			0	24	3.6		

3.8 weight percent PP-g-PS, 24.3 weight percent PP, and 13.0 weight percent EBR. Comparative Example 5 used the acrylonitrile-butadiene-styrene (ABS) resin obtained as CYCLOLAC ® Z-48 from General Electric Company and dried for 4 hours at 210 ° F before use. Comparative Example 6 used the polycarbonate/ABS blend obtained as CYCOLOY ® GPB2800 from General Electric Company. Comparative Example 7 used the acrylic-styrene-acrylonitrile (ASA) terpolymer obtained as GELOY ® CR7010 from General Electric Company. Comparative Example 8 used the polycarbonate resin obtained as LEXAN ® PK2870 from General Electric Company. Comparative Example 9 used the poly(arylene ether) resin obtained as NORYL ® BN9003 from General Electric Company. Comparative Example 10 used the polycarbonate-poly(butylene terephthalate) blend obtained as XENOVY ® 1403B from General Electric Company.

[0090]

Melt strength is a critical property for blow molding because it dictates the maximum size of parts, processing consistency, and the size of the processing window. In blow molding, a semi-solid tube of the molded material (a parison) is extruded through a ring-shaped die. The extruded tube must maintain its integrity and semi-solid state while it is extruded and hanging in place as the mold closes around it. Melt strength can thus be measured in terms of a hang time, which may be defined as the time required for a parison of specific volume and geometry to sag/stretch a predetermined distance. A longer hang time corresponds to a higher melt strength. For these experiments, the hang time test used an APV Blow Molder with a 2.1 pound shot capacity. Test conditions included a 2.5 inch diameter low work screw with 24:1 ratio of parison length to outer diameter; a single cardioid head design; a step mold; a screw speed of 25 rotations per minute (rpm); a die gap of 35%; a blow air pressure of 80 psi; and a mold temperature of 80 ° C. Three measurements were conducted for each composition, and the ranges of values obtained are presented in Table 5. The results show that the composition exhibits a much longer hang time than the commercially available materials. This indicates that the composition is suitable for blow molding large parts.

[t11]

Table 5

	hang time (sec)
Ex. 29	30-35
Comp. Ex. 5	8-9
Comp. Ex. 6	11-13
Comp. Ex. 7	15-18
Comp. Ex. 8	5-6
Comp. Ex. 9	9-11
Comp. Ex. 10	9-11

EXAMPLE 30

[0091] This example illustrates that excellent property balances can be obtained even when the composition does not include a polypropylene-polystyrene graft copolymer. The formulation was compounded and properties were measured as described in Examples 1-20, above. Formulation details and properties are given in Table 6, below.

[t12]

Table 6

	Ex. 30
COMPOSITION	
PPE	24.00
xPS	31.07
SBS	10.00
SEBS H1043	10.00
PP, PD403	10.00
EPR	14.93
PROPERTIES	
Flexural Modulus, 23°C, 1/8" (psi)	255,100
Flexural Strength at Yield, 23°C, 1/8" (psi)	7,522
HDT, 66 psi, 1/8" (°F)	233.6
HDT, 264 psi, 1/8" (°F)	190.2
Notched Izod, 23°C (ft-lb/in)	12.1
Notched Izod, -30°C (ft-lb/in)	9.4
Unnotched Izod, 23°C (ft-lb/in)	24
Energy to Failure, 23°C, 7.5 mph (ft-lb)	18.29
Total Energy, 23°C, 7.5 mph (ft-lb)	26.76
Energy to Failure, -30°C, 7.5 mph (ft-lb)	21.07
Total Energy, -30°C, 7.5 mph (ft-lb)	28.48
Energy to Failure, -30°C, 5 mph (ft-lb)	20.88
Total Energy, -30°C, 5 mph (ft-lb)	28.65
Tensile Strength at Yield, 23°C (psi)	4,676
Tensile Strength at Break, 23°C (psi)	4,288
Tensile Elongation at Break, 23°C (%)	68.87

EXAMPLES 31-40

[0092] These examples further illustrate that excellent property balances can be obtained even when the composition does not include a polypropylene-polystyrene graft copolymer. They also illustrate the low sample-to-sample variability of key properties. Formulations were compounded and properties were measured as described in Examples 1-20, above. Where given, standard deviations are derived from measurements on five samples. Formulations details and properties are given in Table 7, below.

[t13]

Table 7

	Ex. 31	Ex. 32	Ex. 33	Ex. 34
COMPOSITION				
PPE	27.0	30.0	21.0	18.0
xPS	0.0	0.0	0.0	0.0
HIPS	18.0	20.0	14.0	12.0
SBS	15.0	15.0	5.0	15.0
SEBS H1043	6.7	10.0	10.0	10.0
PP, PD403	20.0	20.0	30.0	40.0
EBR	13.3	5.0	20.0	5.0
PROPERTIES				
HDT, 66 psi, 1/8" (°F)	234.5	245.4	215.4	201.8
std. dev. (°F)	2.55	1.00	2.76	2.21
HDT, 264 psi, 1/8" (°F)	154.1	174.1	139.9	137.8
std. dev. (°F)	1.99	4.96	0.05	0.87
Notched Izod, 23°C (ft-lb/in)	11.1	11.7	12.4	12.2
std. dev. (ft-lb/in)	0.2	0.1	0.3	0.2
Notched Izod, -30°C (ft-lb/in)	9.8	8.3	12.3	6
std. dev. (ft-lb/in)	0.1	0.2	0.4	0.2
Energy to Failure, 23°C, 7.5 mph (ft-lb)	16.98	17.88	16.01	16.55
std. dev. (ft-lb)	0.40	0.19	0.43	0.19
Total Energy, 23°C, 7.5 mph (ft-lb)	24.06	26.72	26.25	28.78
std. dev. (ft-lb)	0.62	1.16	0.63	1.40
Energy to Failure, -30°C, 5 mph (ft-lb)	20.66	22.25	20.01	21.31
std. dev. (ft-lb)	0.22	0.22	0.23	0.19
Total Energy, -30°C, 7.5 mph (ft-lb)	29.85	32.04	31.47	32.97
std. dev. (ft-lb)	0.74	1.42	1.75	1.65
Energy to Failure, -30°C, 5 mph (ft-lb)	18.25	22.83	20.01	21.35
std. dev. (ft-lb)	6.45	0.70	0.30	0.51
Total Energy, -30°C, 5 mph (ft-lb)	24.38	31.35	32.75	33.96
std. dev. (ft-lb)	8.64	2.81	0.88	2.60
Flexural Modulus, 23°C, 1/8" (psi)	142,000	180,100	117,800	151,200
std. dev. (psi)	715	1,211	7,031	6,114
Flexural Strength at Yield, 23°C, 1/8" (psi)	5,200	6,580	4,494	5,239
std. dev. (psi)	20	20	265	226
Tensile Strength at Yield, 23°C (psi)	3,945	4,564	3,700	3,950
std. dev. (psi)	78.4	8.4	32.3	26.7
Tensile Strength at Break, 23°C (psi)	4,602	5,112	4,771	4,202
std. dev. (psi)	224	76	306	<0.5
Tensile Elongation at Break, 23°C (%)	213.44	202.06	329.91	379.8
std. dev. (%)	33.0	10.3	58.4	45.1

[t14]

Table 7 (cont.)

	Ex. 35	Ex. 36	Ex. 37	Ex. 38
COMPOSITION				
PPE	22.0	30.0	27.0	30.0
xPS	3.7	0.0	18.0	20.0
HIPS	11.0	20.0	0.0	0.0
SBS	5.0	15.0	5.0	15.0
SEBS H1043	10.0	10.0	10.0	10.0
PP, PD403	40.0	20.0	20.0	20.0
EBR	8.3	5.0	20.0	5.0
PROPERTIES				
HDT, 66 psi, 1/8" (°F)	221.5	244.4	249	254.3
std. dev. (°F)	9.5	2.3	4.5	1.5
HDT, 264 psi, 1/8" (°F)	153.2	179	184.9	195.8
std. dev. (°F)	2.2	3.2	1.75	1.02
Notched Izod, 23°C (ft-lb/in)	11.9	11.7	12.5	10.2
std. dev. (ft-lb/in)	0.2	0.1	0.3	0.2
Notched Izod, -30°C (ft-lb/in)	1.7	8	8.1	4.6
std. dev. (ft-lb/in)	0.2	0.6	0.3	0.3
Energy to Failure, 23°C, 7.5 mph (ft-lb)	16.54	17.59	18.39	19.34
std. dev. (ft-lb)	0.34	0.19	1.05	0.75
Total Energy, 23°C, 7.5 mph (ft-lb)	29.18	26.77	27	27.63
std. dev. (ft-lb)	1.30	0.68	1.49	2.93
Energy to Failure, -30°C, 5 mph (ft-lb)	22.61	22.1	22.14	23.74
std. dev. (ft-lb)	0.87	0.76	0.26	0.22
Total Energy, -30°C, 7.5 mph (ft-lb)	35.28	30.66	31.76	32.29
std. dev. (ft-lb)	2.99	3.04	0.84	1.45
Energy to Failure, -30°C, 5 mph (ft-lb)	23.02	23.84	22.44	23.73
std. dev. (ft-lb)	0.50	0.46	0.37	0.49
Total Energy, -30°C, 5 mph (ft-lb)	35.81	34.02	32.42	33.03
std. dev. (ft-lb)	5.30	1.37	1.20	2.29
Flexural Modulus, 23°C, 1/8" (psi)	175,800	188,300	172,700	211,800
std. dev. (psi)	474	2,028	1,004	1,235
Flexural Strength at Yield, 23°C, 1/8" (psi)	6,332	6,752	6,501	7,787
std. dev. (psi)	57	22	30	30
Tensile Strength at Yield, 23°C (psi)	4,635	4,621	4,746	5,445
std. dev. (psi)	26.1	22.1	17.9	9.9
Tensile Strength at Break, 23°C (psi)	--	5051	4896	5408
std. dev. (psi)	--	92.8	175	111
Tensile Elongation at Break, 23°C (%)	400	186.1	156.48	175.11
std. dev. (%)	<0.5	9.30	31.0	10.3

[t15]

Table 7 (cont.)

	Ex. 39	Ex. 40
COMPOSITION		
PPE	24.0	30.0
xPS	16.0	20.0
HIPS	0.0	0.0
SBS	8.3	15.0
SEBS H1043	10.0	10.0
PP, PD403	36.7	20.0
EBR	5.0	5.0
PROPERTIES		
HDT, 66 psi, 1/8" (°F)	241.6	254.5
<i>std. dev. (°F)</i>	<i>0.64</i>	<i>1.4</i>
HDT, 264 psi, 1/8" (°F)	173.4	195.6
<i>std. dev. (°F)</i>	<i>2.62</i>	<i>0.85</i>
Notched Izod, 23°C (ft-lb/in)	10.3	9.9
<i>std. dev. (ft-lb/in)</i>	<i>0.3</i>	<i>0.1</i>
Notched Izod, -30°C (ft-lb/in)	1.3	5.5
<i>std. dev. (ft-lb/in)</i>	<i>0.1</i>	<i>0.2</i>
Energy to Failure, 23°C, 7.5 mph (ft-lb)	17.89	18.55
<i>std. dev. (ft-lb)</i>	<i>0.54</i>	<i>0.42</i>
Total Energy, 23°C, 7.5 mph (ft-lb)	26.9	27.11
<i>std. dev. (ft-lb)</i>	<i>2.41</i>	<i>1.92</i>
Energy to Failure, -30°C, 5 mph (ft-lb)	19.78	23.37
<i>std. dev. (ft-lb)</i>	<i>5.99</i>	<i>0.2</i>
Total Energy, -30°C, 7.5 mph (ft-lb)	24.81	33.34
<i>std. dev. (ft-lb)</i>	<i>10.08</i>	<i>0.92</i>
Energy to Failure, -30°C, 5 mph (ft-lb)	22.46	23.23
<i>std. dev. (ft-lb)</i>	<i>1.72</i>	<i>0.34</i>
Total Energy, -30°C, 5 mph (ft-lb)	30.27	32.88
<i>std. dev. (ft-lb)</i>	<i>5.67</i>	<i>1.17</i>
Flexural Modulus, 23°C, 1/8" (psi)	197,100	211,100
<i>std. dev. (psi)</i>	<i>1,339</i>	<i>1,933</i>
Flexural Strength at Yield, 23°C, 1/8" (psi)	7,246	7,801
<i>std. dev. (psi)</i>	<i>63</i>	<i>92</i>
Tensile Strength at Yield, 23°C (psi)	5,198	5,415
<i>std. dev. (psi)</i>	<i>21.4</i>	<i>50.7</i>
Tensile Strength at Break, 23°C (psi)	5,095	5,394
<i>std. dev. (psi)</i>	<i>125</i>	<i>37</i>
Tensile Elongation at Break, 23°C (%)	233.8	176.3
<i>std. dev. (%)</i>	<i>26.6</i>	<i>9.2</i>

EXAMPLES 41-47

[0093]

These examples further illustrate the excellent property balances and low sample-to-sample variability of key properties exhibited by the composition. Formulations were compounded and properties were measured as described in Examples 1-20, above. Where given, standard deviations are derived from measurements on five samples. Formulation details and properties are given in Table 8, below.

[t16]

Table 8

	Ex. 41	Ex. 42	Ex. 43	Ex. 44
COMPOSITION				
PPE	27.00	30.00	21.00	18.00
HIPS	18.00	20.00	14.00	12.00
SBS	15.00	15.00	5.00	15.00
SEBS H1043	6.67	10.00	10.00	10.00
PP, PD403	20.00	20.00	30.00	40.00
EBR	13.33	5.00	20.00	5.00
PROPERTIES				
HDT, 66 psi, 1/8" (°F)	234.5	245.4	215.4	201.8
HDT, 264 psi, 1/8" (°F)	154.1	174	139.9	137.8
Notched Izod, 23°C (ft-lb/in)	11.1	11.7	12.4	12.2
Notched Izod, -30°C (ft-lb/in)	9.8	8.3	12.3	6.0
Energy to Failure, 23°C, 7.5 mph (ft-lb)	16.98	17.88	16.01	16.55
<i>std. dev. (ft-lb)</i>	<i>0.40</i>	<i>0.19</i>	<i>0.43</i>	<i>0.19</i>
Total Energy, 23°C, 7.5 mph (ft-lb)	24.06	26.72	26.25	28.78
<i>std. dev. (ft-lb)</i>	<i>0.62</i>	<i>1.16</i>	<i>0.63</i>	<i>1.40</i>
Energy to Failure, -30°C, 7.5 mph (ft-lb)	20.66	22.25	20.01	21.31
<i>std. dev. (ft-lb)</i>	<i>0.22</i>	<i>0.22</i>	<i>0.23</i>	<i>0.19</i>
Total Energy, -30°C, 7.5 mph (ft-lb)	29.85	32.04	31.47	32.97
<i>std. dev. (ft-lb)</i>	<i>0.74</i>	<i>1.42</i>	<i>1.75</i>	<i>1.65</i>
Energy to Failure, -30°C, 5 mph (ft-lb)	18.25	22.83	20.01	21.35
<i>std. dev. (ft-lb)</i>	<i>6.45</i>	<i>0.699</i>	<i>0.30</i>	<i>0.51</i>
Total Energy, -30°C, 5 mph (ft-lb)	24.38	31.35	32.75	33.96
<i>std. dev. (ft-lb)</i>	<i>8.64</i>	<i>2.81</i>	<i>0.88</i>	<i>2.60</i>
Flexural Modulus, 23°C, 1/8" (psi)	142,000	180,100	117,800	151,200
Flexural Strength at Yield, 23°C, 1/8" (psi)	5,200	6,580	4,494	5,239
Tensile Strength at Yield, 23°C (psi)	3,945	4,564	3,700	3,950
Tensile Strength at Break, 23°C (psi)	4,602	5,112	4,771	4,202
Tensile Elongation at Break, 23°C (%)	213.44	202.06	329.91	379.8

[t17]

Table 8 (cont.)

	Ex. 45	Ex. 46	Ex. 47
COMPOSITION			
PPE	18.00	22.00	30.00
HIPS	6.00	11.00	20.00
xPS	6.00	3.67	0.00
SBS	15.00	5.00	15.00
SEBS H1043	10.00	10.00	10.00
PP, PD403	40.00	40.00	20.00
EBR	5.00	8.33	5.00
PROPERTIES			
HDT, 66 psi, 1/8" (°F)	214.6	221.5	244.4
HDT, 264 psi, 1/8" (°F)	147	153.2	179
Notched Izod, 23°C (ft-lb/in)	12.4	11.9	11.7
Notched Izod, -30°C (ft-lb/in)	2.6	1.7	8
Energy to Failure, 23°C, 7.5 mph (ft-lb)	14.57	16.54	17.59
<i>std. dev. (ft-lb)</i>	<i>0.25</i>	<i>0.34</i>	<i>0.19</i>
Total Energy, 23°C, 7.5 mph (ft-lb)	25.72	29.18	26.77
<i>std. dev. (ft-lb)</i>	<i>0.74</i>	<i>1.30</i>	<i>0.68</i>
Energy to Failure, -30°C, 7.5 mph (ft-lb)	20.87	22.61	22.1
<i>std. dev. (ft-lb)</i>	<i>0.11</i>	<i>0.87</i>	<i>0.76</i>
Total Energy, -30°C, 7.5 mph (ft-lb)	29.59	35.28	30.66
<i>std. dev. (ft-lb)</i>	<i>1.79</i>	<i>2.99</i>	<i>3.04</i>
Energy to Failure, -30°C, 5 mph (ft-lb)	20.13	23.02	23.84
<i>std. dev. (ft-lb)</i>	<i>1.71</i>	<i>0.50</i>	<i>0.46</i>
Total Energy, -30°C, 5 mph (ft-lb)	27.41	35.81	34.02
<i>std. dev. (ft-lb)</i>	<i>5.66</i>	<i>5.30</i>	<i>1.37</i>
Flexural Modulus, 23°C, 1/8" (psi)	165,200	175,800	188,30
Flexural Strength at Yield, 23°C, 1/8" (psi)	5,873	6,332	6,752
Tensile Strength at Yield, 23°C (psi)	4,069	4,635	4,621
Tensile Strength at Break, 23°C (psi)	4,287	--	5,051
Tensile Elongation at Break, 23°C (%)	375	400	186.1

EXAMPLE 48, COMPARATIVE EXAMPLE 11

[0094]

This example and comparative example illustrate the improved property balance and reduced sample-to-sample property variability exhibited by samples molded the composition. Compositions and properties are given in Table 9, below.

[t18]

Table 9

	Ex. 48	C. Ex.11
COMPOSITION		
PPE	16.20	16.20
xPS	20.20	20.20
HIPS	0.00	0.00
SBS	11.40	11.40
SEBS H1043	6.30	0.00
SEBS, G1652	0.00	6.30
PP, PD403	33.80	33.90
EPR	6.30	6.30
PP-g-PS	5.90	5.90
PROPERTIES		
HDT, 66 psi, 1/8" (°F)	229	226
<i>std. dev., 3 samples (°F)</i>	1.8	4.3
HDT, 264 psi, 1/8" (°F)	170	166
<i>std. dev., 3 samples (°F)</i>	1.1	3.7
Notched Izod, 23°C (ft-lb/in)	8.9	5.1
<i>std. dev., 5 samples (ft-lb/in)</i>	0.3	1.5
Notched Izod, -30°C (ft-lb/in)	2.5	2.6
<i>std. dev., 5 samples (ft-lb/in)</i>	0.1	0.6
Energy to Failure, 23°C, 7.5 mph (ft-lb)	19.2	18.8
<i>std. dev., 5 samples (ft-lb)</i>	0.2	1.1
Total Energy, 23°C, 7.5 mph (ft-lb)	32.4	24.6
<i>std. dev., 5 samples (ft-lb)</i>	0.4	7.2
Energy to Failure, -30°C, 7.5 mph (ft-lb)	14.7	8.0
<i>std. dev., 5 samples (ft-lb)</i>	2.4	6.3
Total Energy, -30°C, 7.5 mph (ft-lb)	17.0	8.7
<i>std. dev., 5 samples (ft-lb)</i>	3.0	7.0
Energy to Failure, -30°C, 5 mph (ft-lb)	21.9	9.0
<i>std. dev., 5 samples (ft-lb)</i>	1.0	8.3
Total Energy, -30°C, 5 mph (ft-lb)	29.6	10.5
<i>std. dev., 5 samples (ft-lb)</i>	4.4	10.7
Flexural Modulus, 23°C, 1/8" (kpsi)	221	190
<i>std. dev., 5 samples (kpsi)</i>	1	16
Flexural Strength at Yield, 23°C, 1/8" (psi)	7,300	6,429
<i>std. dev., 5 samples (psi)</i>	32	410
Tensile Strength at Yield, 23°C (psi)	5,060	4,577
<i>std. dev., 3 samples (psi)</i>	19	177
Tensile Strength at Break, 23°C (psi)	5,079	4,333
<i>std. dev., 5 samples (psi)</i>	65	285
Tensile Elongation at Break, 23°C (%)	273	155
<i>std. dev., 5 samples (psi)</i>	12	82

EXAMPLES 49–52

[0095] These examples illustrate the effect of the ratio of poly(arylene ether) to poly(alkenyl aromatic) on the balance of properties, in particular the balance of flexural modulus and heat distortion temperature. The results, presented in Table 10, show that increasing the xPS:PPE ratio results in increasing mechanical properties such as flexural modulus and flexural strength, while decreasing thermal properties, such as heat distortion temperature, and toughness properties, such as Izod notched impact

strength and energy to failure.

[t19]

Table 10

	Ex. 49	Ex. 50	Ex. 51	Ex. 52
COMPOSITION				
PP, PD403	14.30	14.30	14.30	14.30
EPR	7.26	7.26	7.26	7.26
PP-g-PS	3.93	3.93	3.93	3.93
SBS	5.76	5.76	5.76	5.76
SEBS	5.96	5.96	5.96	5.96
xPS	16.00	20.00	25.00	30.00
PPE	46.79	42.80	37.80	32.79
CALCULATED PROPERTIES				
Flexural Modulus, 23°C, 1/8" (psi)	304,974	311,018	318,495	325,910
Flexural Strength at Yield, 23°C, 1/8" (psi)	10,087	10,135	10,192	10,245
HDT, 66 psi, 1/8" (°F)	290.4	281.2	269.8	258.4
HDT, 264 psi, 1/8" (°F)	234.9	228.6	220.5	212.5
Notched Izod, 23°C (ft-lb/in)	5.95	5.74	5.48	5.24
Notched Izod, -30°C (ft-lb/in)	1.76	1.73	1.69	1.66
Unnotched Izod, 23°C, 1/8" (ft-lb/in)	13.14	12.30	11.31	10.41
Energy to Failure, 23°C, 7.5 mph (ft-lb)	10.35	9.16	7.78	6.51
Total Energy, 23°C, 7.5 mph (ft-lb)	14.44	12.81	10.92	9.17
Energy to Failure, -30°C, 7.5 mph (ft-lb)	6.51	5.66	4.75	3.99
Total Energy, -30°C, 7.5 mph (ft-lb)	4.11	3.41	2.75	2.27
Energy to Failure, -30°C, 5 mph (ft-lb)	3.92	3.69	3.16	2.49
Total Energy, -30°C, 5 mph (ft-lb)	4.80	4.43	3.74	2.93
Tensile Strength at Yield, 23°C (psi)	5,900	6,008	6,141	6,272
Tensile Strength at Break, 23°C (psi)	5,577	5,672	5,787	5,901
Tensile Elongation at Break, 23°C (%)	13.9	13.7	13.4	13.1

EXAMPLES 53-58, COMPARATIVE EXAMPLES 12-17

[0096] These examples illustrate the improved impact strength exhibited by the examples of composition, containing an unhydrogenated block copolymer, when compared to comparative examples lacking an unhydrogenated block copolymer. Formulations were compounded and properties were measured as described in Examples 1-20, above. Components are the same as those described in Table 1, except that the poly(arylene ether) (PPE) had an intrinsic viscosity of 0.46 dL/g as measured at 25 ° C in chloroform. "Additives" refers to a 1:1:3 weight ratio blend of magnesium oxide, zinc sulfide, and tridodecyl phosphite. Formulation details and properties are given in Table 11, below.

[0097] The results show that Examples 53-58, containing an unhydrogenated block

copolymer, exhibit superior Notched Izod at 23 ° C, Notched Izod at -30 ° C, Energy to Maximum Load at -30 ° C and 7.5 mph, and Energy to Maximum Load at -30 ° C and 5 mph, compared to Comparative Examples 12-17, respectively, not containing an unhydrogenated block copolymer.

[t20]

Table 11

	C. Ex. 12	Ex. 53	C. Ex. 13	Ex. 54
COMPOSITION				
PP, PD403	32.00	32.00	27.00	27.00
EBR	0.00	0.00	5.00	5.00
SBS	0.00	5.00	0.00	5.00
SEBS H1043	8.00	8.00	8.00	8.00
xPS	30.00	25.00	30.00	25.00
HIPS	0.00	0.00	0.00	0.00
PPE 0.46 IV	30.00	30.00	30.00	30.00
Additives	0.00	0.25	0.25	0.25
PROPERTIES				
Flexural Modulus, 23°C, 1/8" (psi)	315,500	274,600	275,600	251,700
<i>std. dev.</i>	1,572	1,170	1,819	4,106
Flexural Strength at Yield, 23°C, 1/8" (psi)	11,700	10,180	10,450	9,413
<i>std. dev.</i>	65	30	50	99
HDT, 264 psi, 1/8" (°F)	215.5	207.2	212.9	203.1
<i>std. dev.</i>	1.6	3.3	2.7	2.4
HDT, 66 psi, 1/8" (°F)	265.4	262.4	260.3	261.3
<i>std. dev.</i>	1.2	2.1	1.2	2.5
Notched Izod, 23°C (ft-lb/in)	0.7	1.8	1.7	5.2
<i>std. dev.</i>	0.2	0	0.1	0.5
Notched Izod, -30°C (ft-lb/in)	0.5	1.0	0.6	1.6
<i>std. dev.</i>	0.1	0.1	0.1	0.3
Energy to Maximum Load, 23°C, 7.5 mph (ft-lb)	5.95	20.09	20.43	19.75
<i>std. dev.</i>	4.27	0.37	0.89	0.74
Energy to Failure, 23°C, 7.5 mph (ft-lb)	6.33	30.34	28.14	29.5
<i>std. dev.</i>	4.45	2.27	2.93	0.25
Energy to Maximum Load, -30°C, 7.5 mph (ft-lb)	1.4	5.75	3.7	15.24
<i>std. dev.</i>	0.41	5.35	2.99	6.99
Energy to Failure, -30°C, 7.5 mph (ft-lb)	1.51	6.07	3.94	16.43
<i>std. dev.</i>	0.42	5.56	3.11	8.15
Energy to Maximum Load, -30°C, 5 mph (ft-lb)	1.02	5.42	3.49	15.15
<i>std. dev.</i>	0.3	5.8	1.3	8.9
Energy to Failure, -30°C, 5 mph (ft-lb)7669	1.13	5.65	3.62	15.62
<i>std. dev.</i>	0.26	5.90	1.34	9.14
Tensile Strength at Yield, 23°C (psi)	7,669	6,910	7,072	6,464
<i>std. dev.</i>	100.7	18.2	355.1	26.6
Tensile Strength at Break, 23°C (psi)	5,999	5,595	5,716	5,437
<i>std. dev.</i>	92.7	24.7	164.7	15.6
Tensile Elongation at Break, 23°C (%)	36.27	69.30	49.66	75.04
<i>std. dev.</i>	3.93	9.38	19.60	4.65

[t21]

Table 11 (cont.)

	C. Ex. 14	Ex. 55	C. Ex. 15	Ex. 56
COMPOSITION				
PP, PD403	40.00	40.00	36.00	36.00
EBR	0.00	0.00	4.00	4.00
SBS	0.00	4.00	0.00	4.00
SEBS H1043	10.00	10.00	10.00	10.00
xPS	0.00	0.00	0.00	0.00
HIPS	20.00	16.00	20.00	16.00
PPE 0.46 IV	30.00	30.00	30.00	30.00
Additives	0.00	0.25	0.25	0.25
PROPERTIES				
Flexural Modulus, 23°C, 1/8" (psi)	233,100	220,700	207,200	195,800
<i>std. dev.</i>	2,085	3,046	969	2,280
Flexural Strength at Yield, 23°C, 1/8" (psi)	8,720	8,125	7,706	7,246
<i>std. dev.</i>	20	138	19	49
HDT, 264 psi, 1/8" (°F)	184.7	175.1	177.3	164.3
<i>std. dev.</i>	4.9	5.5	1.4	3.1
HDT, 66 psi, 1/8" (°F)	259.2	254.7	258.4	251
<i>std. dev.</i>	2.0	1.0	2.4	1.9
Notched Izod, 23°C (ft-lb/in)	2.3	3.6	5.9	7.6
<i>std. dev.</i>	0.1	0.1	0.5	0.1
Notched Izod, -30°C (ft-lb/in)	1.1	1.5	1.7	2.4
<i>std. dev.</i>	0.1	0.1	0.2	0.2
Energy to Maximum Load, 23°C, 7.5 mph (ft-lb)	18.26	18.62	19.27	18.53
<i>std. dev.</i>	5.35	0.62	0.38	0.36
Energy to Failure, 23°C, 7.5 mph (ft-lb)	25.53	29.24	28.89	28.90
<i>std. dev.</i>	9.10	1.13	1.17	1.05
Energy to Maximum Load, -30°C, 7.5 mph (ft-lb)	12.80	22.07	18.36	23.54
<i>std. dev.</i>	7.77	3.62	9.18	1.65
Energy to Failure, -30°C, 7.5 mph (ft-lb)	13.31	28.50	23.25	29.11
<i>std. dev.</i>	7.99	8.86	13.10	5.11
Energy to Maximum Load, -30°C, 5 mph (ft-lb)	16.22	22.32	16.62	19.73
<i>std. dev.</i>	7.50	0.94	4.63	3.90
Energy to Failure, -30°C, 5 mph (ft-lb)	18.06	27.92	17.65	24.99
<i>std. dev.</i>	9.30	6.19	5.30	7.58
Tensile Strength at Yield, 23°C (psi)	6,058	5,708	5,606	5,229
<i>std. dev.</i>	35.3	25.8	11.4	7.1
Tensile Strength at Break, 23°C (psi)	5,254	5,259	5,136	5,152
<i>std. dev.</i>	96.5	25.8	112.7	64.1
Tensile Elongation at Break, 23°C (%)	117.35	189.37	135.09	204.03
<i>std. dev.</i>	21.03	11.59	29.21	8.26

[t22]

Table 11 (cont.)

	C. Ex. 16	Ex. 57	C. Ex. 17	Ex. 58
COMPOSITION				
PP, PD403	32.00	27.00	27.00	22.00
EBR	0.00	0.00	5.00	5.00
SBS	0.00	5.00	0.00	5.00
SEBS H1043	8.00	8.00	8.00	8.00
xPS	0.00	0.00	0.00	0.00
HIPS	15.00	15.00	15.00	15.00
PPE 0.46 IV	45.00	45.00	45.00	45.00
Additives	0.00	0.25	0.25	0.25
PROPERTIES				
Flexural Modulus, 23°C, 1/8" (psi)	252,600	247,500	224,600	222,400
<i>std. dev.</i>	2,699	1,810	1,910	2,037
Flexural Strength at Yield, 23°C, 1/8" (psi)	9,577	9,350	8,537	8,382
<i>std. dev.</i>	49	25	55	19
HDT, 264 psi, 1/8" (°F)	200.9	198.7	205.7	209.1
<i>std. dev.</i>	5.4	9.2	2.6	4.2
HDT, 66 psi, 1/8" (°F)	286.6	282.5	291.1	289.3
<i>std. dev.</i>	2.4	6.6	1.4	0.6
Notched Izod, 23°C (ft-lb/in)	2.0	3.0	4.6	6.8
<i>std. dev.</i>	0.1	0.1	0.3	0.4
Notched Izod, -30°C (ft-lb/in)	1.3	1.6	2.1	2.4
<i>std. dev.</i>	0.1	0.2	0.2	0.2
Energy to Maximum Load, 23°C, 7.5 mph (ft-lb)	21.90	21.25	20.28	20.41
<i>std. dev.</i>	0.43	0.46	0.55	0.63
Energy to Failure, 23°C, 7.5 mph (ft-lb)	28.48	28.72	27.2	27.6
<i>std. dev.</i>	1.37	1.05	2.83	1.02
Energy to Maximum Load, -30°C, 7.5 mph (ft-lb)	15.31	20.09	25.85	26.96
<i>std. dev.</i>	5.62	5.28	2.05	0.23
Energy to Failure, -30°C, 7.5 mph (ft-lb)	15.82	20.77	30.72	31.66
<i>std. dev.</i>	5.72	5.42	6.04	1.99
Energy to Maximum Load, -30°C, 5 mph (ft-lb)	13.62	19.62	24.56	24.83
<i>std. dev.</i>	5.21	7.81	1.61	1.30
Energy to Failure, -30°C, 5 mph (ft-lb)	13.97	21.72	29.27	29.39
<i>std. dev.</i>	5.31	9.59	4.06	3.19
Tensile Strength at Yield, 23°C (psi)	6,473	6,451	6,156	5,953
<i>std. dev.</i>	41.6	16.7	21.2	11.7
Tensile Strength at Break, 23°C (psi)	5,733	5,702	5,605	5,551
<i>std. dev.</i>	120.4	102.7	52.2	57.4
Tensile Elongation at Break, 23°C (%)	56.24	47.21	58.36	40.86
<i>std. dev.</i>	6.07	3.49	4.53	3.02

[0098]

While the invention has been described with reference to a preferred embodiment, it will be understood by those skilled in the art that various changes may be made and equivalents may be substituted for elements thereof without departing from the scope of the invention. In addition, many modifications may be made to adapt a particular situation or material to the teachings of the invention without departing from scope thereof. Therefore, it is intended that the invention not be limited to the particular embodiment disclosed as the best mode contemplated for carrying out this invention, but that the invention will include all embodiments falling within the scope

[illegible]

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